

# SAE Baja '24 Capstone Team

## Presentation 2

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Joey Barta, Lars Jensen, Seth Deluca  
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# Front Team

Abraham Plis, Evan Kamp, Bryce Fennell

# Project Description



NAU SAE Baja 2020-2021

## What is SAE Baja?

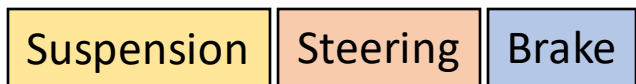
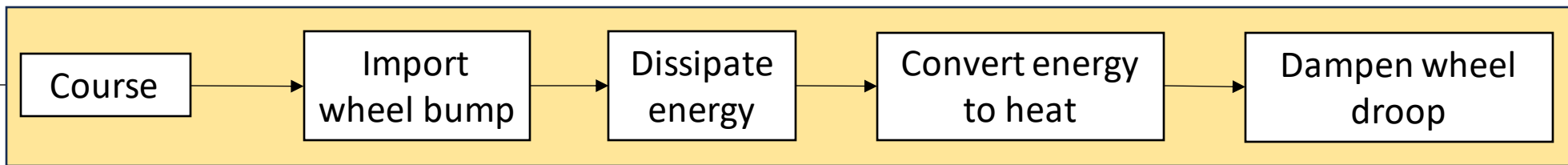
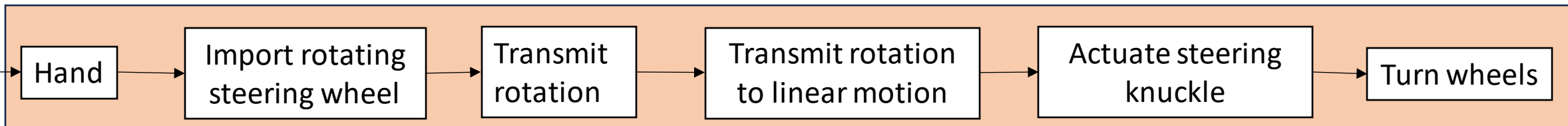
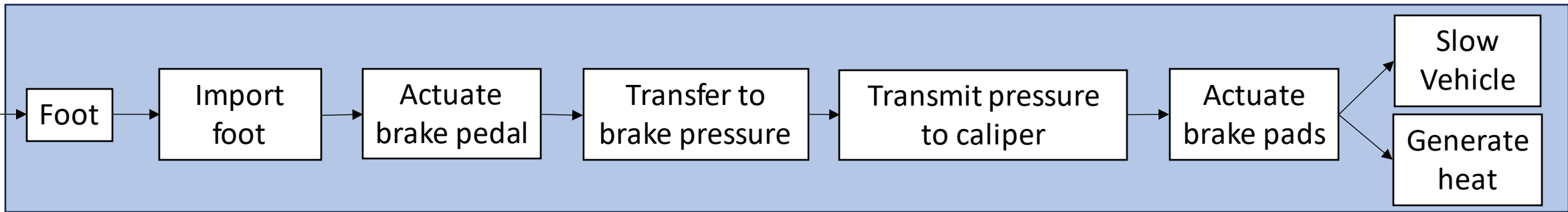
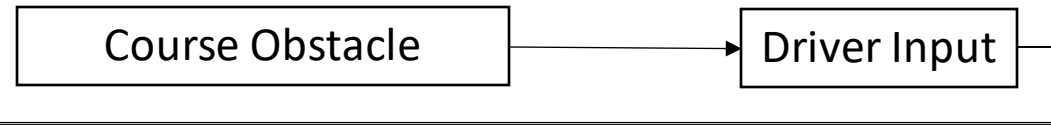
The Society of Automotive Engineers (SAE) Baja Collegiate Design Series is an engineering challenge for students to design and build a single-seat, all-terrain vehicle.

- Compete against other universities
- 13 members total, 4 sub-teams
  - Front End, Rear End, Frame, Drivetrain
- Sponsors: WL GORE, Monster Energy
- Successful performance puts NAU on the map, strengthens internal Baja knowledge, and grows NAU Baja industry sponsorship connections










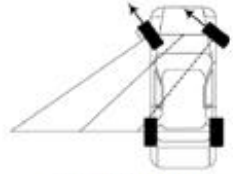
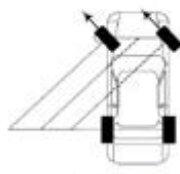
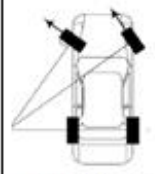
# Black Box Model



# Functional Model





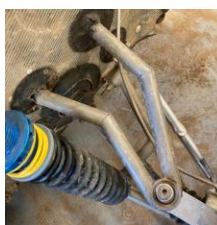




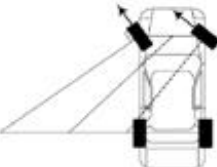
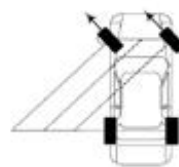
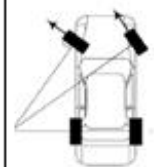


# Concept Generation

Subsystem	Variants		
	1	2	3
Scrub Radius	 <p>Positive</p>	 <p>Negative</p>	 <p>Zero</p>
Control Arm Geometry	 <p>A Arm</p>	 <p>J Arm</p>	 <p>Wishbone</p>
Control Arm Construction	 <p>CNC</p>	 <p>Welded</p>	 <p>Carbon</p>
Steering Arrangement	 <p>Anti-Ackerman</p>	 <p>Parallel</p>	 <p>Pro-Ackerman</p>

- **Sub-systems** were generated by researching the required attributes of a functioning SAE Baja vehicle
- **Variants** were generated based off prior literature reviews and calculations performed in Presentation 1

# Concept Generation

Subsystem	Variants		
	1	2	3
Scrub Radius	 <p>Positive</p>	 <p>Negative</p>	 <p>Zero</p>
Control Arm Geometry	 <p>A Arm</p>	 <p>J Arm</p>	 <p>Wishbone</p>
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Steering Arrangement	 <p>Anti-Ackerman</p>	 <p>Parallel</p>	 <p>Pro-Ackerman</p>

## Sub-System Influence

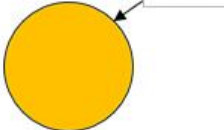
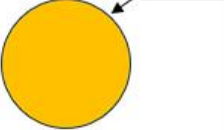
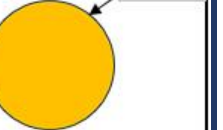
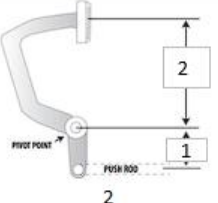
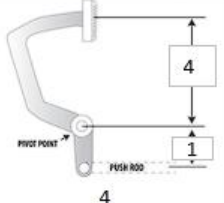
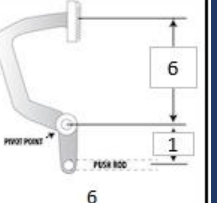





Steering control under hard braking/acceleration

Stresses seen by the arm during dynamic operation

Ease of Fabrication and Cost

Turning Radius of Vehicle

# Concept Generation

Subsystem	Variants		
	1	2	3
Master Cylinder Bore Size	 1/2" $\varnothing$	 5/8" $\varnothing$	 3/4" $\varnothing$
Brake Pedal Ratio	 2	 4	 6
Camber During Suspension Bump	<b>POSITIVE CAMBER</b>  Loss	<b>NEGATIVE CAMBER</b>  Gain	<b>NEUTRAL CAMBER</b>  No-Change
Shock Mount Location	 UCA	 LCA	

## Sub-System Influence

Clamping Force and Caliper Size

Mechanical Advantage On Brake Pedal

Roll Performance/Stability

Geometry of 4WD Axle Path in Front



# Engineering Calculations – Front 1

## Equations, Tools, & Examples

**Side view swing arm height given percentage anti dive Formula**

Side View Swing Arm Height = Percentage Anti Dive Front / (((Percentage front braking) \* (1 / Side View Swing Arm Length) / (Height of CG above road / Wheelbase of Vehicle)))

$$svsa_{height} = \%antidive_{front} / ((\%Braking_{front}) * (1 / svsa_{length}) / (h / b))$$

Percentage Anti Dive Front [%antidive <sub>front</sub> ]	20	+10%	-10%
Percentage front braking [%Braking <sub>front</sub> ]	60	+10%	-10%
Side View Swing Arm Length [svsa <sub>length</sub> ]	37.2	+10%	-10%
Height of CG above road [h]	22	+10%	-10%
Wheelbase of Vehicle [b]	62	+10%	-10%
Side view swing arm height given percentage anti dive [svsa <sub>height</sub> ]	4.4		

Equation/online platform used to calculate anti-dive characteristics based on a variety of predetermined vehicle dimensions [90]

**General range of the values**

Parameters	Front	Rear
Camber @Jounce 5"	-2deg – 3deg	0 - 4 deg
Caster	10-12 deg	0
KPI	7-10 deg	0
Toe in and Toe out	0 – 2deg (in or out)	0 – 2deg (in or out)
Scrub radius	2 – 5in	0
Roll center height	11in – 15in	7in – 12in
C.G of vehicle	23 – 28 in	

Example of ideal spec ranges for SAE Baja vehicles to guide this year's suspension design [91]

ADAMS CAR TUTORIAL SERIES

Chapter Two – SUSPENSION ANALYSIS.

SUSPENSION GEOMETRY      SAE BAJA 2021      SAE SUPRA 2021

ADAMS Suspension software provides a “free” alternative to Lotus Shark (should the need arise), application for comp. package [92]

# Engineering Calculations – Front 2 Scrub Radius

Scrub Radius - Wheel Torque Under Braking		
Variant	Diagram	Result
1 - Positive		64 lbf*ft
2 - Negative		64 lbf*ft
3 - Zero		0 lbf*ft

To calculate the influence of scrub radius on toe characteristics, we can use the following governing equations & assumptions:

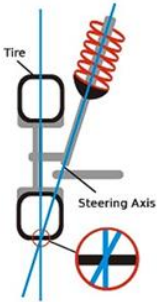
$$F_{braking} = \frac{\text{Weight of Car}}{2} * (\text{Coeff. Friction Tire to Asphalt})$$

$$T_{wheel} = F_{braking} * D_{Moment Arm}$$

Weight of Car = 550 lbs. (with driver)  
 Coeff. = 0.7 (worst case)  
 Moment Arm = 4 in.

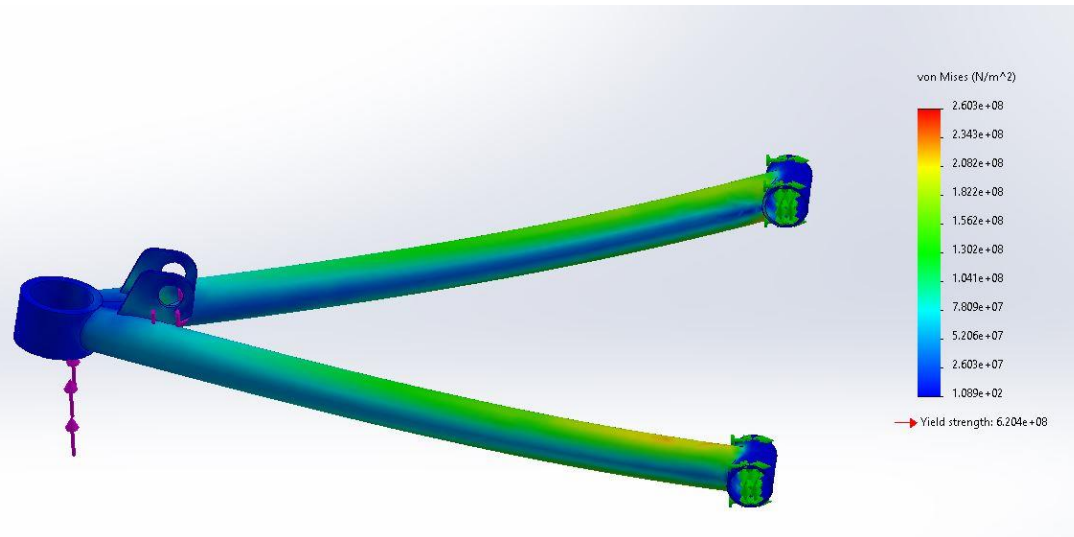


**Zero Scrub Has Least Steering Influence!**

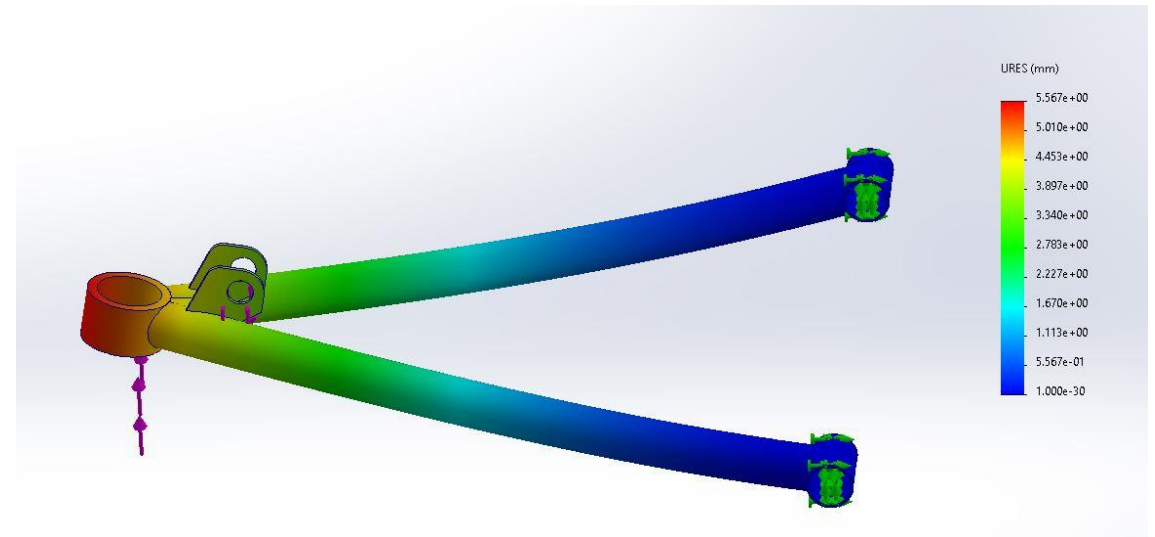


# Engineering Calculations – Front 3

## Control Arm Geometry – A Arm Minimized Complication



Developed stress on front upper control arm





Displacement on front upper control arm

**Assumptions:** 550lb vehicle enduring full weight on a single wheel falling from ~3 feet  
**Importance:** Of all geometries simulated, A-Arm has least complicated stress interaction

SolidWorks analysis of stresses on the **Upper Control Arm** during a maximum force event. Resulting FOS of 2.38 meaning the **Design Passes!**

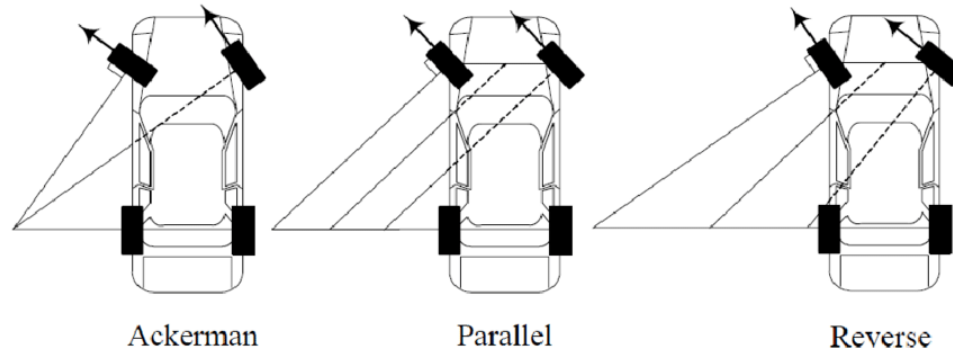
# Engineering Calculations – Front 4

## Control Arm Construction

Type of Control Arm	Material Cost	Design Time	Manufacturing Time	Other Benefits
Welded 	4'x4 control arms 1"OD with 1/16" ID Using 4130 Steel  <b>\$40x4 = \$160</b>	1 hour CAD for both the upper and lower control arm. 10 minutes to mirror to passenger side <b>TOTAL 2hr 10min</b>	1 hour of jiggling with 45 minutes of welding <b>TOTAL 1hr 45min</b>	Additional Adjustability with welded
CNC Aluminum 	2'x1'x2" billet for each Control Arm  <b>\$600x4 = \$2400</b>	4 hour CAD for both upper and lower control arm. 10 minutes to mirror to passenger side <b>TOTAL 8hr 10min</b>	2 hours of Programming 2 hours of Machining <b>TOTAL 4hr</b>	If done correctly could be Lightweight

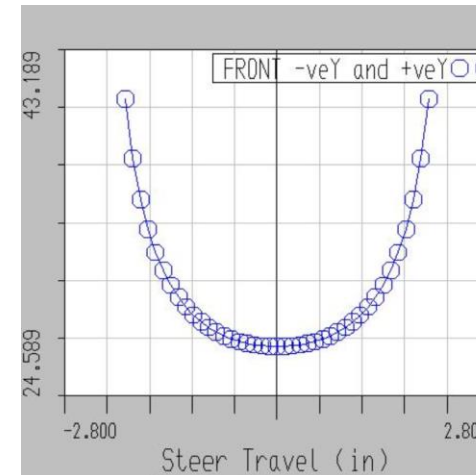
# Engineering Calculations – Front 5

## Steering Arrangement



*Preliminary Measurements Using Lotus Shark*

Inner wheel angle ( $\delta_i$ )	50°
Outer wheel angle ( $\delta_o$ )	28.4°
$\delta_{avg}$	39.2°
Rear wheel to center of gravity (a2)	32

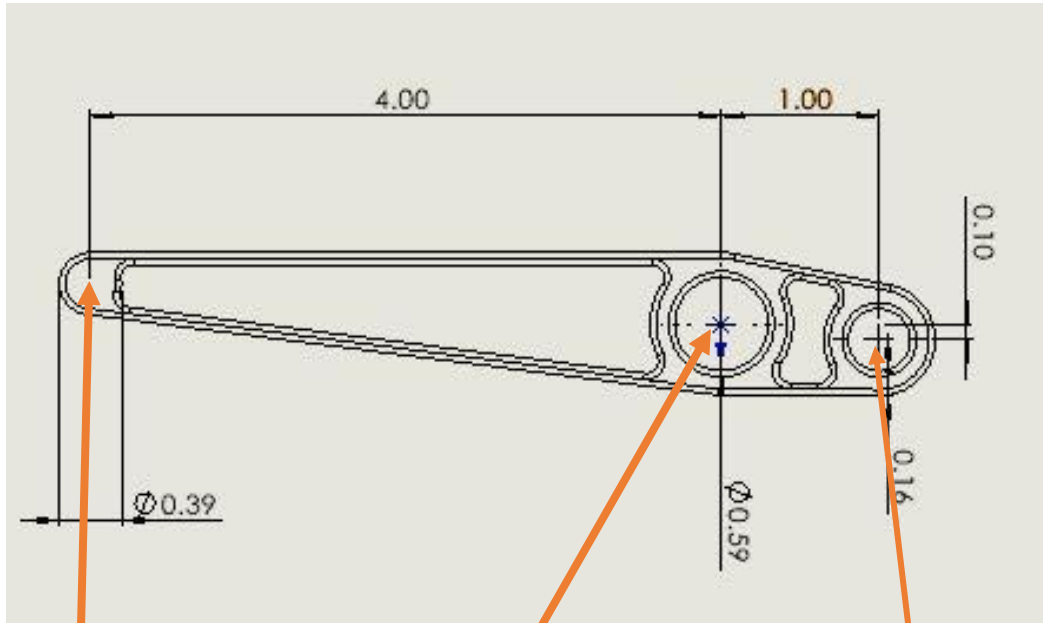


*Results*

Percent Ackerman Used	43.189%
Projected Turning Radius (R)	6.93ft

# Engineering Calculations – Front 6

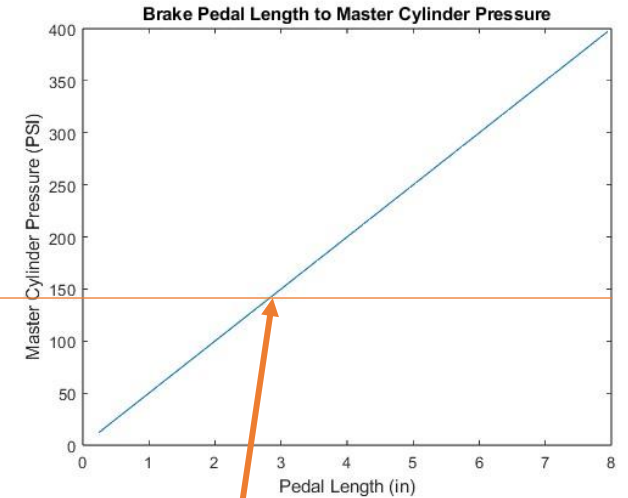
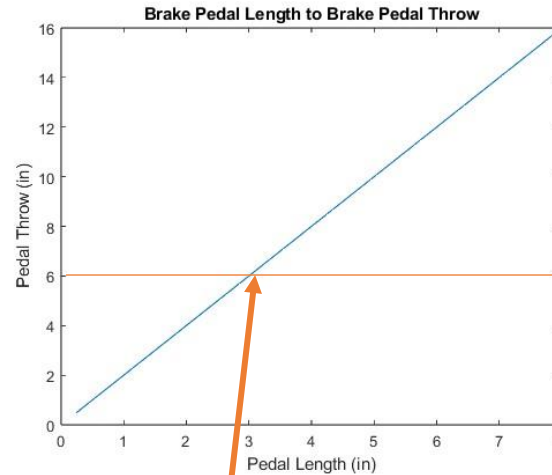
## Brake Pedal Length



Brake Pedal Center Mount

Pivot Point

Master Cylinder Mount



Optimal pedal throw per driver requirements, Resulting master cylinder hydraulic pressures

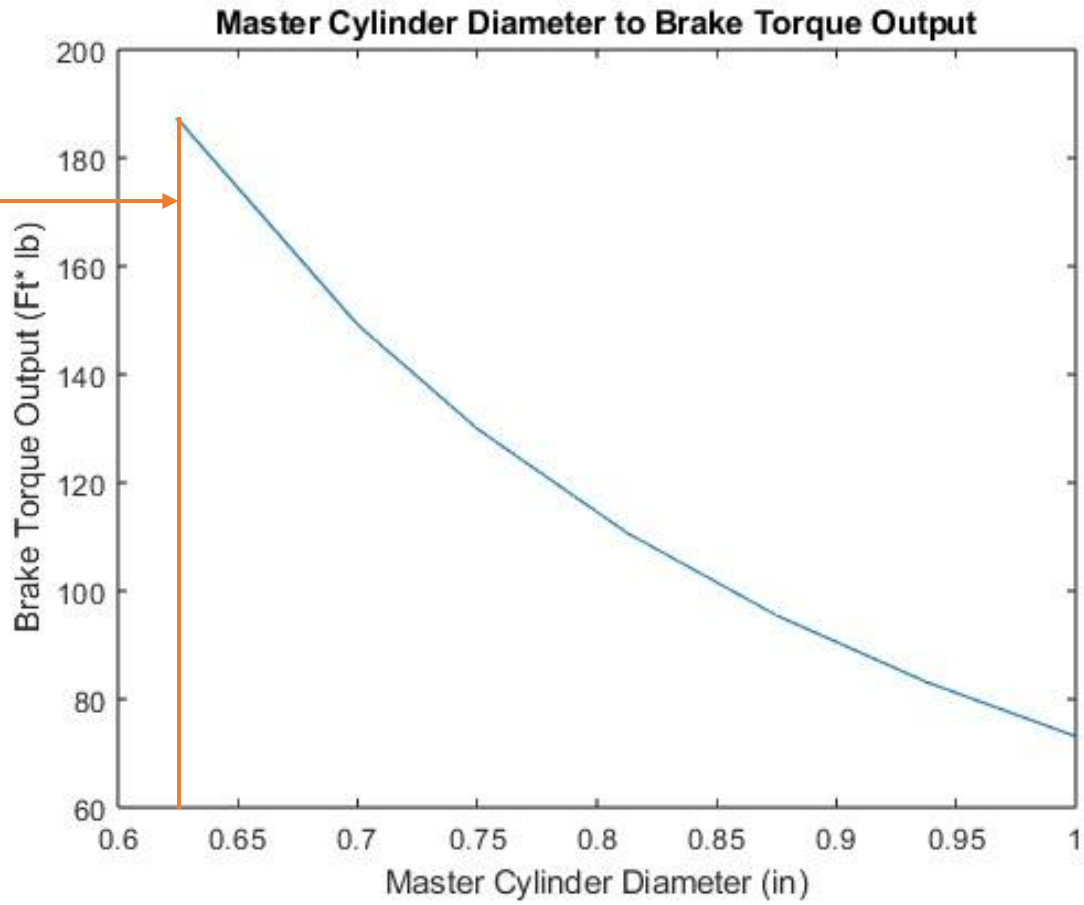
A brake pedal throw to master cylinder throw ratio of 4:1 will provide maximum power transfer with minimal pedal motion

# Engineering Calculations – Front 7

## Master Cylinder Bore Size

Maximum  
brake torque  
(5/8" bore) at  
~190 ft\*lb.

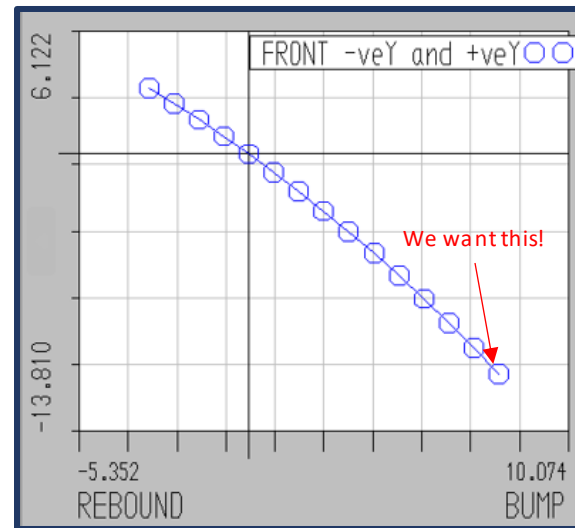
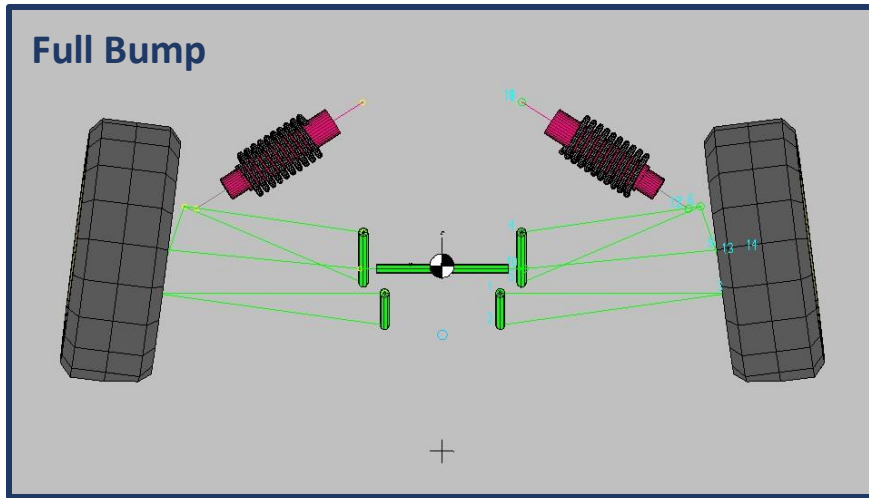
Optimizing for  
the maximum  
braking output  
for master  
cylinder ID  
compared to  
**maximum**  
braking force



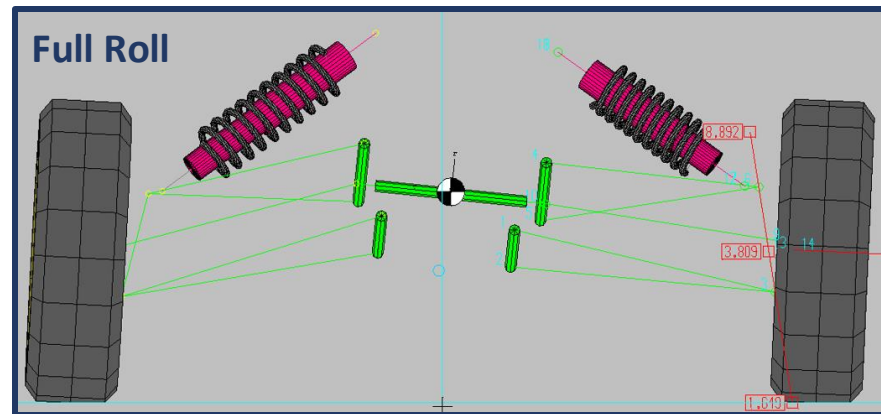
Tilton Brake Master Cylinder, 5/8" Bore

# Engineering Calculations – Front 8

## Camber During Suspension Bump



Camber gain refers to how much negative camber the wheels gain during compression (bump)



More negative camber gained during compression helps maintain tire contact and prevent wheels from tipping over during roll

Camber During Bump		
Variant	Diagram	Result
1 - Gain		Better Roll Performance
2 - Loss		Worse Roll Performance
3 - No Change		Subpar Roll Performance

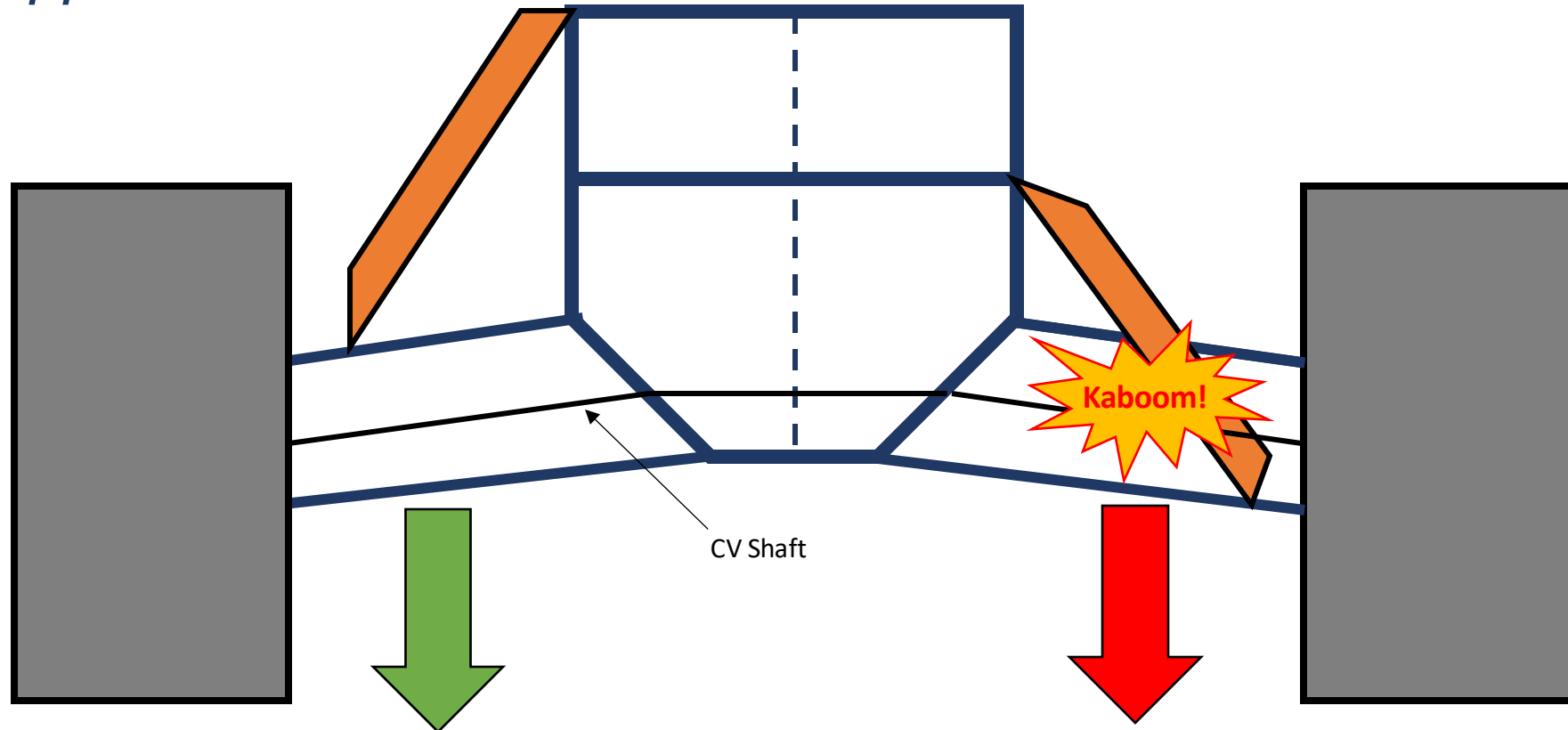


# Engineering Calculations – Front 9

## Shock Mount Location

*To Upper Control Arm*

*To Lower Control Arm*



**No Interference!!**

**Interference!!**

# Concept Evaluation

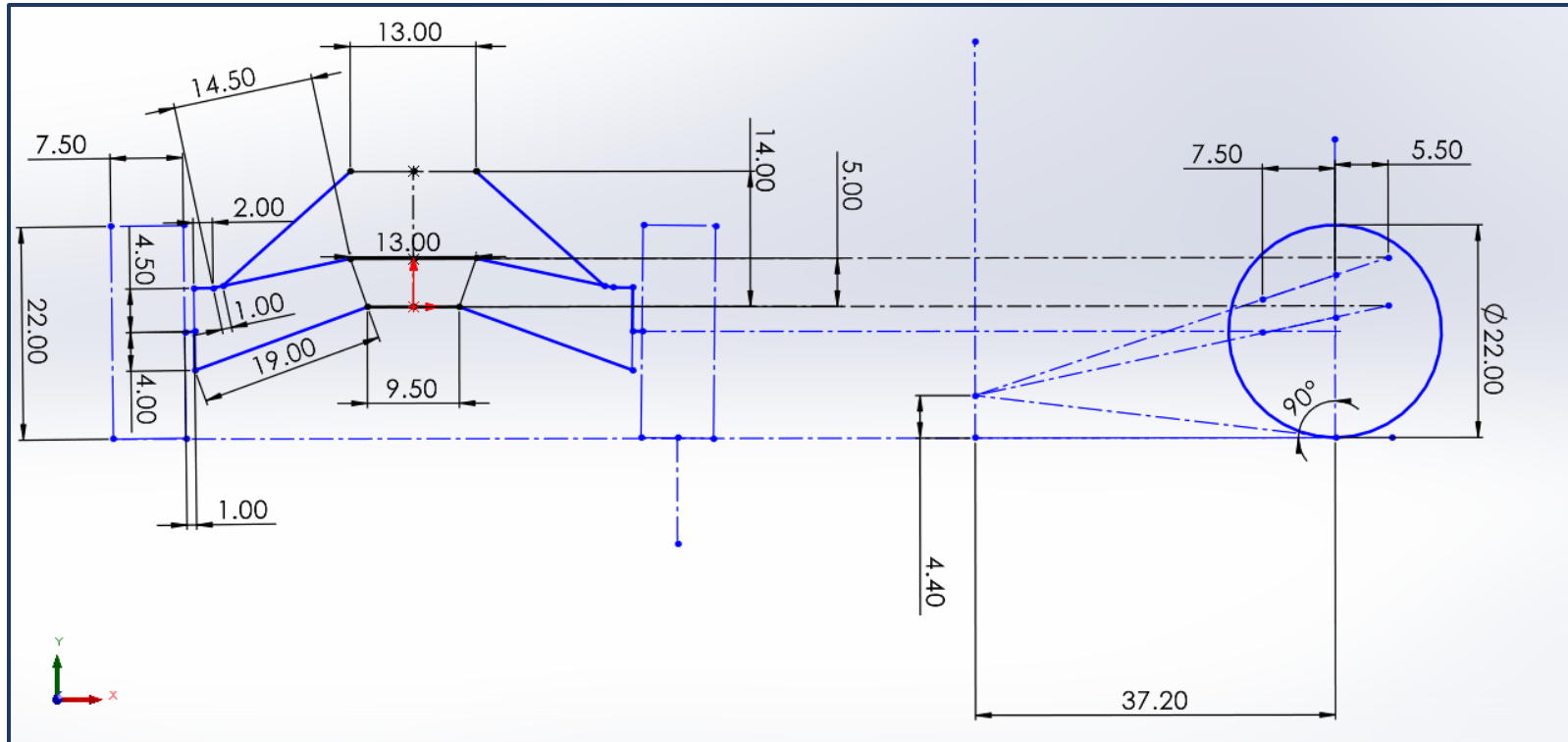
Subsystem	Variants					
	1	Rating	2	Rating	3	Rating
Scrub Radius	Positive	X	Negative	X	Zero	✓
Control Arm Geometry	A Arm	✓	J Arm	X	Wishbone	X
Control Arm Construction	CNC	X	Welded	✓	Carbon	X
Steering Arrangement	Anti-Ackerman	X	Parallel	X	Ackerman	✓
Master Cylinder Bore	1/2"	X	5/8"	✓	3/4"	X
Brake Pedal Ratio	2	X	4	✓	6	X
Camber During Suspension Bump	Loss	X	Gain	✓	No-Change	X
Shock Mount Location	UCA	✓	LCA	X		

# Final Design Discussion

Subsystem	Variants					
	1	Rating	2	Rating	3	Rating
Scrub Radius	Positive	X	Negative	X	Zero	✓
Control Arm Geometry	A Arm	✓	J Arm	X	Wishbone	X
Control Arm Construction	CNC	X	Welded	✓	Carbon	X
Steering Arrangement	Anti-Ackerman	X	Parallel	X	Ackerman	✓
Master Cylinder Bore	1/2"	X	5/8"	✓	3/4"	X
Brake Pedal Ratio	2	X	4	✓	6	X
Camber During Suspension Bump	Loss	X	Gain	✓	No-Change	X
Shock Mount Location	UCA	✓	LCA	X		

# Final Design Visualization

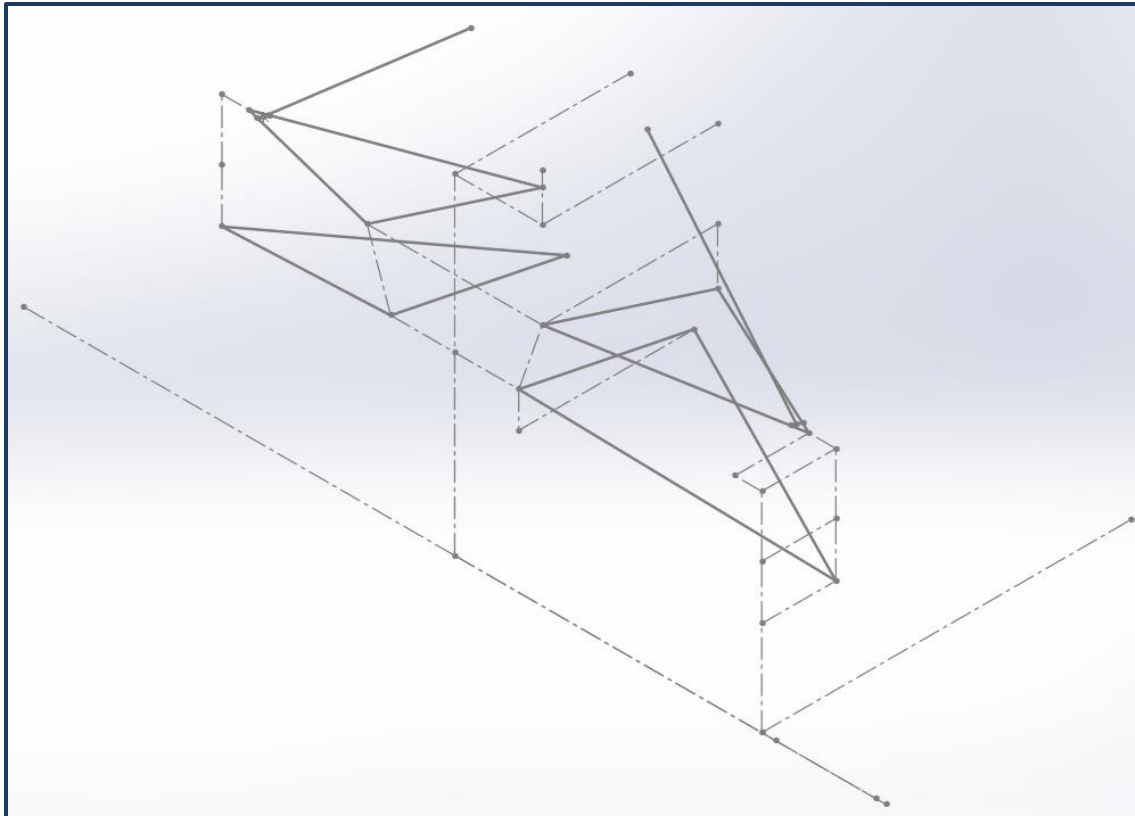
## Initial Steering Geometry Calculations



- 2D geometry calculations performed in accordance with *Race Car Vehicle Dynamics* and other sources [93, 94]
- Convert to 3D points for Shark Processing...

# Final Design Visualization

## Initial Steering Geometry Calculations

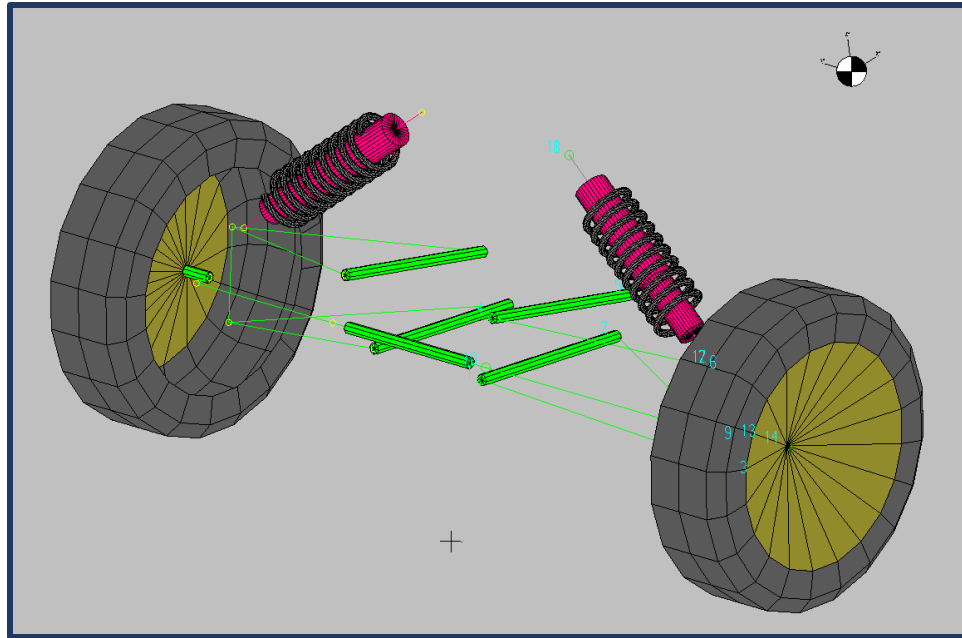


SolidWorks				
	Coordinate Description	X (Driver + Passenger -)	Y (Up + Down -)	Z (Towards Front + Towards Rear -)
Drivers Side	UCA Front Pivot	6.5	18.06	0
	UCA Rear Pivot	6.5	13.9	-13
	LCA Front Pivot	4.75	13.06	0
	LCA Rear Pivot	4.75	10.42	-13
	UCA Ball Joint	20.77	15.51	-5.5
	LCA Ball Joint	22.77	7.01	-5.5
	UCA Shock Mount	19.77	15.54	-5.57
	Frame Shock Mount	6.54	26.77	-7.75
Passenger Side	UCA Front Pivot	-6.5	18.06	0
	UCA Rear Pivot	-6.5	13.9	-13
	LCA Front Pivot	-4.75	13.06	0
	LCA Rear Pivot	-4.75	10.42	-13
	UCA Ball Joint	-20.77	15.51	-5.5
	LCA Ball Joint	-22.77	7.01	-5.5
	UCA Shock Mount	-19.77	15.54	-5.57
	Frame Shock Mount	-6.54	26.77	-7.75

- 2D calculations transferred to 3D sketch
- Initial hardpoints tabulated for easier import into Shark
- Iteration, iteration, iteration...

# Final Design Visualization

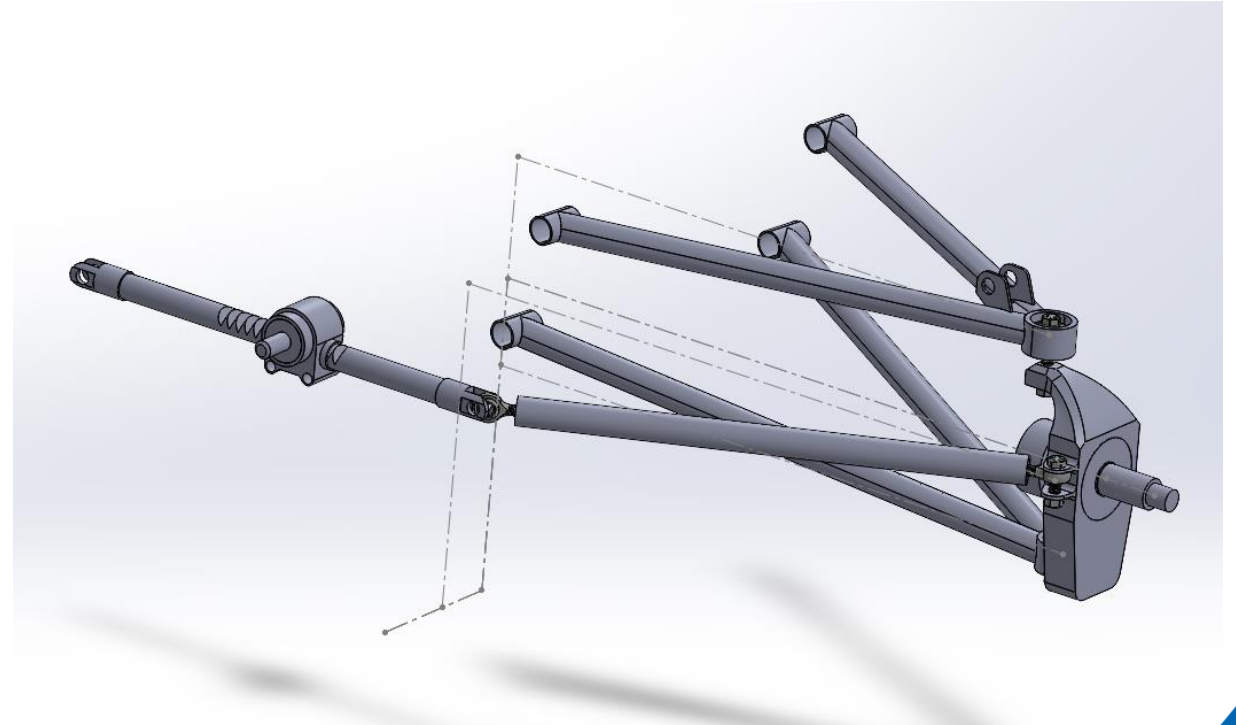
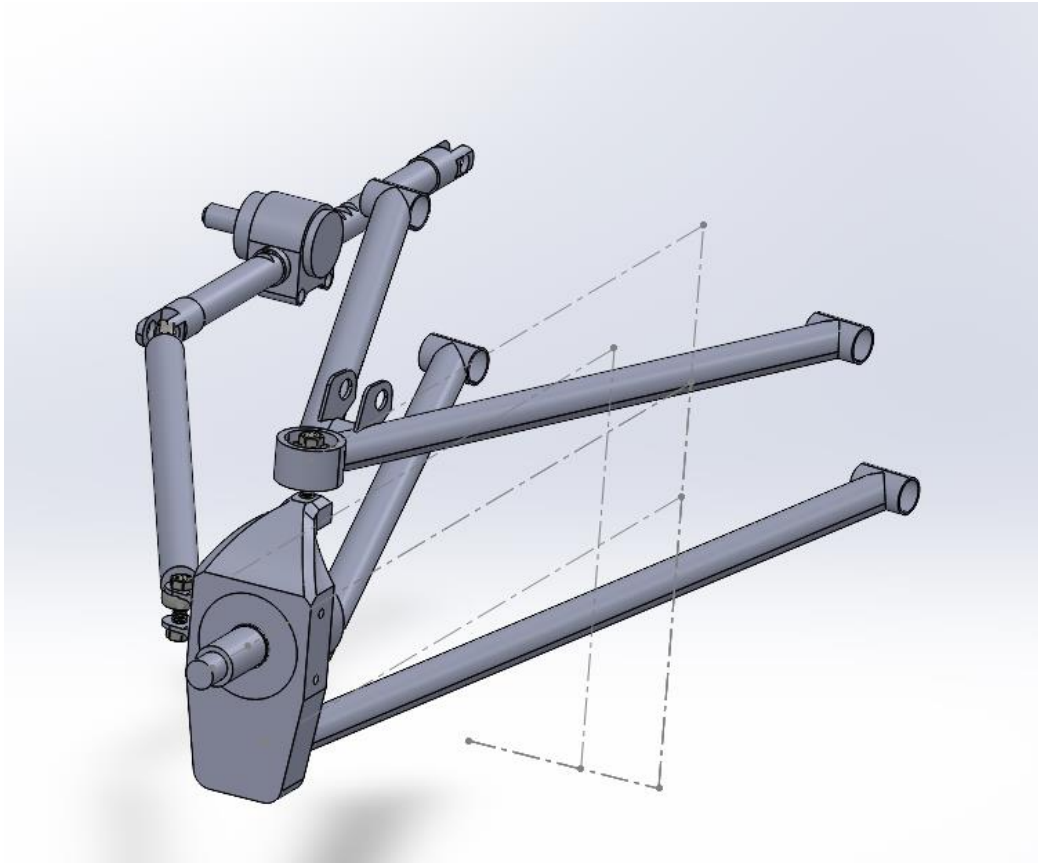
Finalized Front End  
Geometry from *Shark*



Upper & Lower Control Arms  
w/ Shock On Frame



# Final Design Visualization



Isometric view of current SolidWorks model for SAE Baja '24 front end





# Project Schedule

## Next Steps:

- **Front:** UCA, LCA, Knuckle, and Steering in CAD
- **Rear:** Trailing Arm & Camber Links in CAD
- **Frame:** Finalize Frame by Halloween (Tabs & All Members)
- **Drive:** Front/Rear Gearboxes & 4WD Belt in CAD, continue work on eCVT

Deadline(s): Rough CAD by 10/31

Project Status: **On-Track** ✓

# Bill of Materials – Front

Steering	Quantity	Costing	Total	Suspension	Quantity	Costing	Total
steering column	1	50	\$ 50.00	upper arm	2	33	\$ 66.00
steering rack	1	200	\$200.00	lower arm	2	27	\$ 54.00
bearing for steering column	2	20	\$ 40.00	ball joints	4	25	\$ 100.00
rod ends	4	15	\$ 60.00	delrin bushing	4	3	\$ 12.00
tie rods	2	45	\$ 90.00	shocks	2	Owned	\$ -
			Total: \$440.00				Total: \$ 232.00
Brake	Quantity	Costing	Total	Drive	Quantity	Costing	Total
caliper	2	180	\$180.00	cv axle	2	Owned	\$ -
master cylinder	1	280	\$280.00	cv bearing	2	15	\$ 30.00
rotor	2	40	\$ 80.00	knuckle	2	300	\$ 600.00
brake lines	10ft	150	\$150.00	hub	2	180	\$ 360.00
brake line fittings	From Kit (~10)	90	\$ 90.00	rim*	2	Owned	\$ -
brake pressure sensor	1	15	\$ 1.00	tire	2	Owned	\$ -
dot 5.1 fluid	32oz	20	\$ 20.00	stud	8	6	\$ 48.00
brake pads	4	Included	\$ -	lugnut	2	12	\$ 24.00
brake pedal	1	110	\$110.00	cotter pin	2	2	\$ 4.00
			Total: \$911.00				Total: \$ 1,066.00

Total Cost Per Unit: \$2649

BOM for SAE Baja '24 Front Team

# Front End Budget

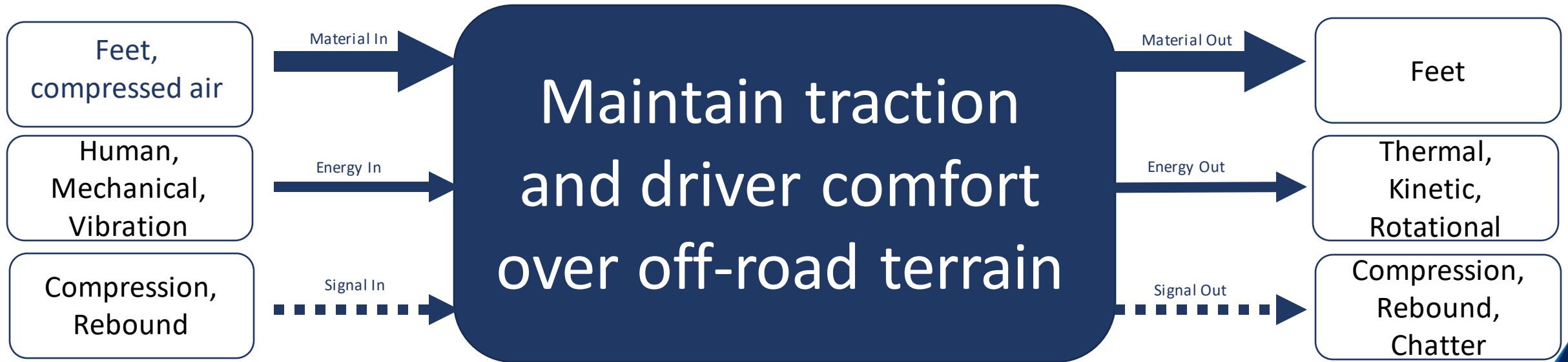
	Category	Relevant Items	Approximated Cost
1	Vehicle Expenses	Brake System Control Arm Materials Rod-ends/Ball Joints Shock Rebuild Knuckle Material/Manufacturing  <b>Estimated Total</b>	\$1,000 \$120 \$50 \$126 \$1600  <b>\$2649</b>
2	Spare Parts	Rod-ends, Bushings, Welding supplies, Hardware	\$500
3	Competition Expenses Front Sub-team	Registration, travel (hotel rooms, vehicle rentals, gas, etc.)	\$1,125
4	Contingency (5%)	Unpredicted Expenses	\$400
		<b>Total</b>	<b>\$4,674</b>

**NAU**

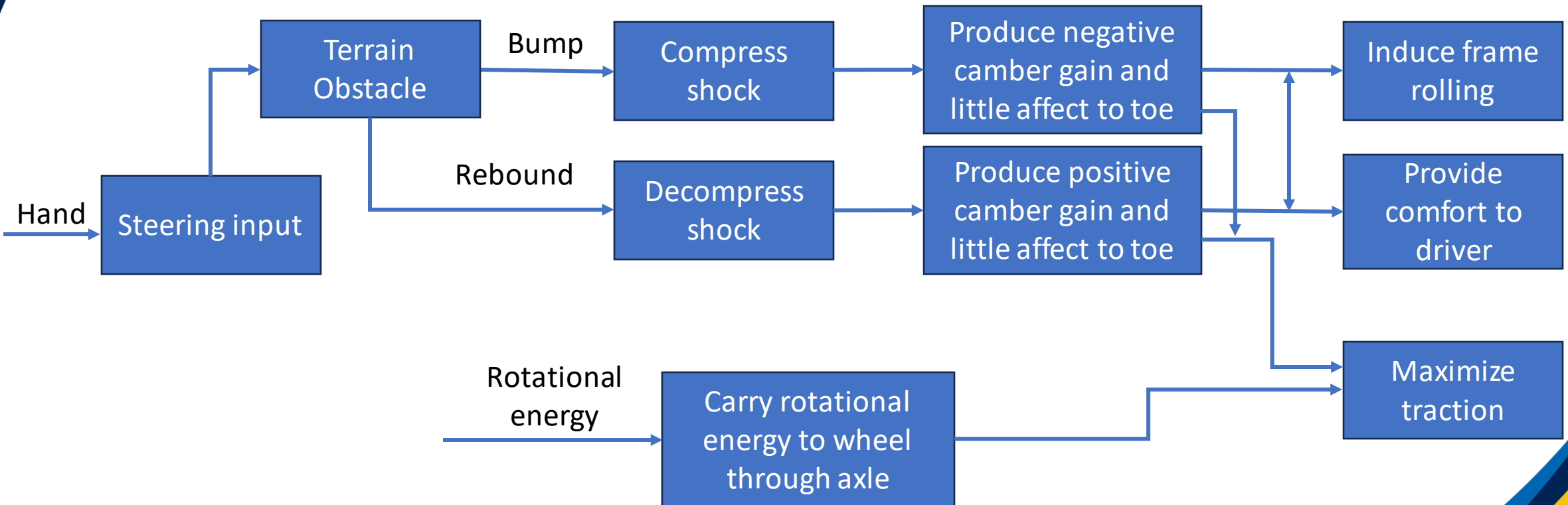
# Rear Team

Seth DeLuca, Joey Barta, Lars Jensen

# Black Box Model - Rear















# Functional Model



# Concept Generation

Concepts generated by researching successful baja teams and the subsystems they use.

Subsystem	Variants		
	1	2	3
<b>Camber</b>	<p><b>POSITIVE CAMBER</b></p>  <p>positive</p>	<p><b>NEGATIVE CAMBER</b></p>  <p>negative</p>	<p><b>NEUTRAL CAMBER</b></p>  <p>neutral</p>
<b>Toe</b>	<p><b>TOE-IN</b></p>  <p>in</p>	<p><b>TOE-OUT</b></p>  <p>out</p>	<p><b>NEUTRAL TOE</b></p>  <p>neutral</p>
<b>Camber Link Material</b>	 <p>Carbon Fiber</p>	 <p>Steel</p>	 <p>Aluminum</p>
<b>Axle types</b>	 <p>CV Axle</p>	 <p>Dogbone</p>	 <p>U-Joint axle</p>

## Sub-System Influence

Cornering performance and traction

Steering characteristics and handling

Weight and strength

Reliability/strength

# Concept Generation

Subsystem	Variants		
	1	2	3
Knuckle Design	 CNC Machined Aluminum	 Steel	 Attach knuckle to trailing arm
Hub	 Aluminum (machined)	 Cast	
hardware	 SS	 Steel	 Ti
Trailing Link Design	 Boxed Sheet Metal	 Steel Tubing	 CNC Machined Aluminum
Wheel dish	 Dish out	 Dish in	

## Sub-System Influence

Production, tunability,  
weight, and strength

Weight, production,  
and strength

Weight and strength at  
joints

EVERYTHING

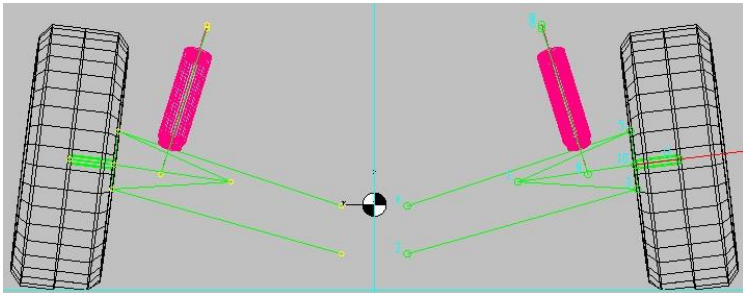
Geometry of 4WD  
Axle Path in Front



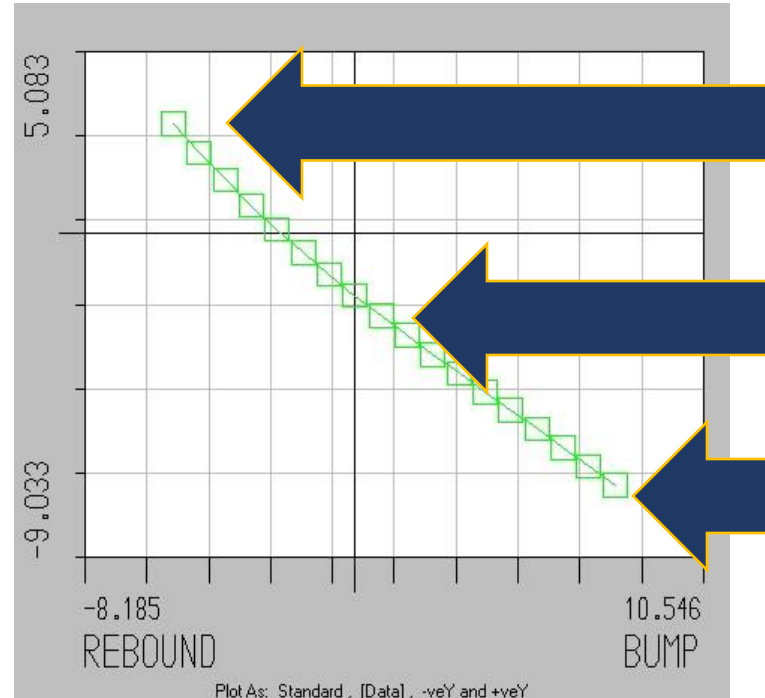
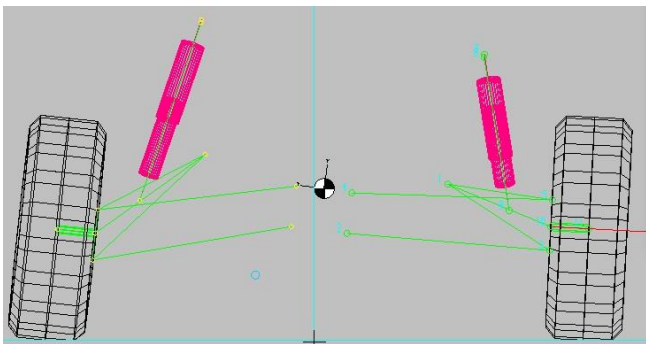
# Engineering Calculations – Rear 1

## Camber

Full Compression



Full Roll



Positive camber at full droop

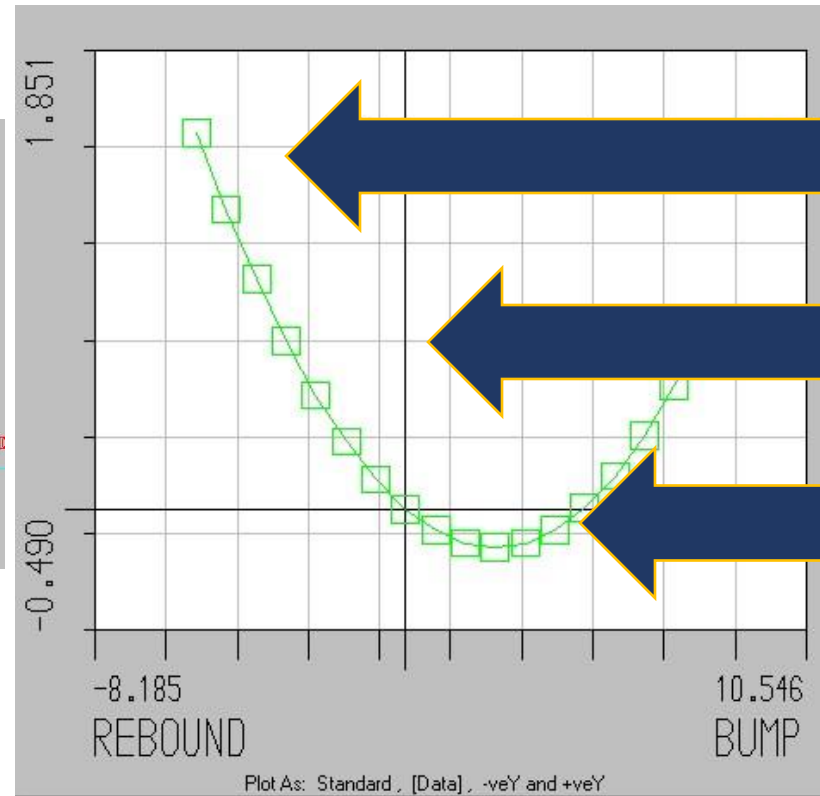
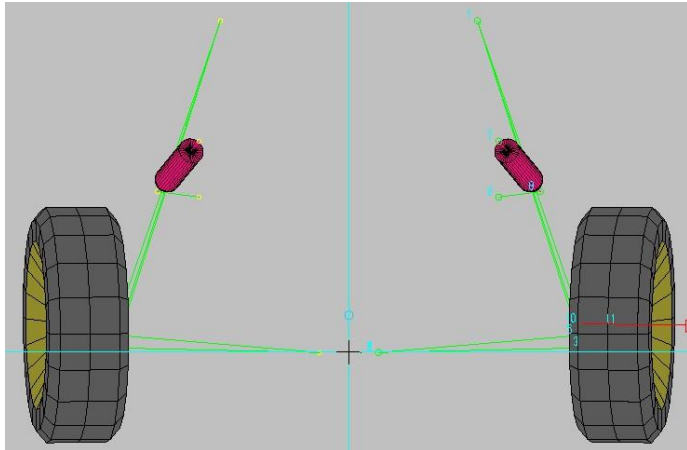
Negative camber at ride height

Negative camber gain

# Engineering Calculations – Rear 2

## Toe

Top view full  
compression

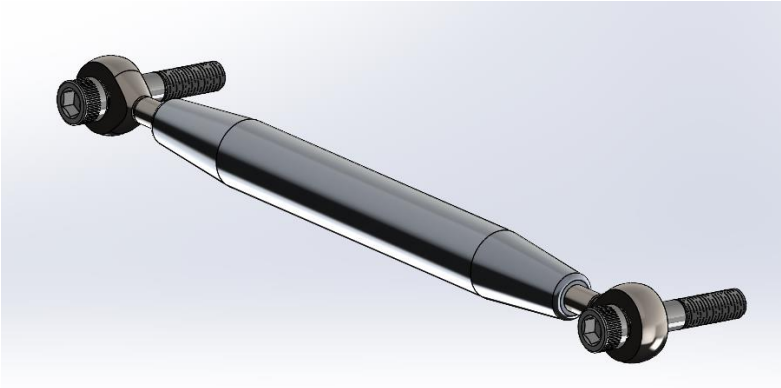


Minor toe out at  
droop  
Zero at ride  
height  
As close to zero  
as possible

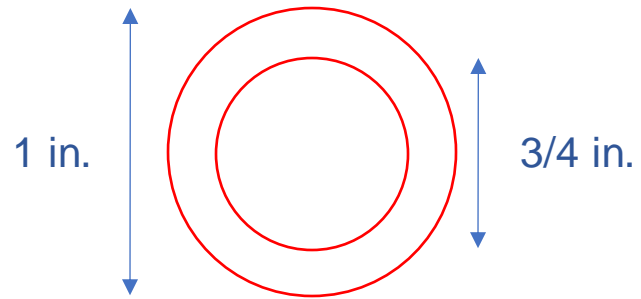
# Engineering Calculations – Rear 3

## Camber link material

Aluminum Camber Link – tapered tube



Length = 18in.



### Assumptions

- Uniform Cross-Section
- Analysis under load (compression)
- No affect from ball joints and screw connections

$$Q_{max} = \frac{2}{3}(r_o^3 - r_i^3) \quad \tau_{max} = \frac{4V}{3A} \left( \frac{r_o^2 + r_o r_i + r_i^2}{r_o^2 + r_i^2} \right) = \frac{4 \times 45lbf}{3 \times 0.3436in^2} (1.48in^2) \gg 258.44psi$$

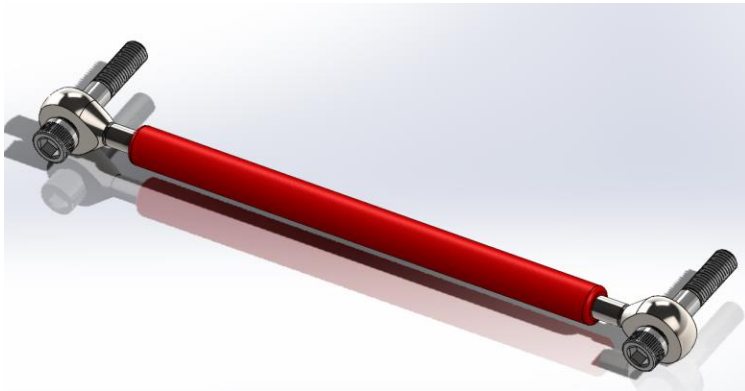
$S_Y$  for 6063 – T6 Aluminum = 31,118 psi

$$FoS = \frac{31,118}{258.44} = 120.4$$

# Engineering Calculations – Rear 3

## Camber link material

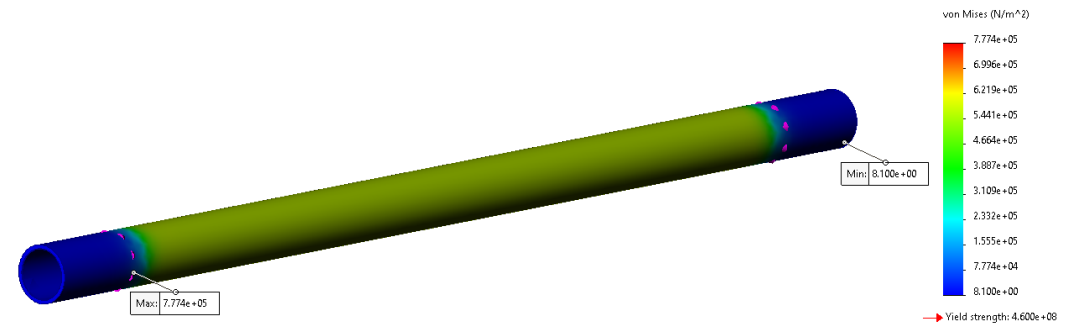
Other Possible options:



Carbon Fiber Camber Link – Hollow uniform cross-section tube with 7075 T6 machined aluminum insert

$$S_{Ut} \text{ for Carbon Fiber} = 650,000 \text{ psi}$$

Note: Carbon Fiber has varying strength in different axis' making it difficult to analyze/compare



Steel Camber Link – uniform cross-section tube

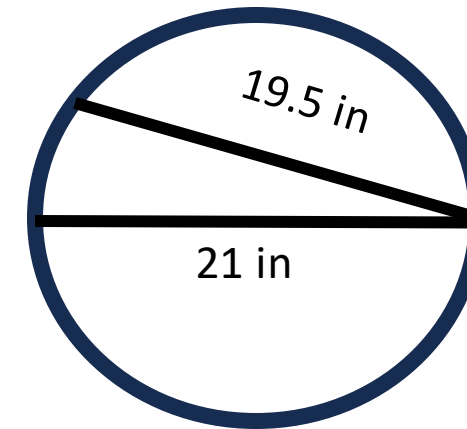
$$S_Y \text{ for 4130 Steel} = 66,717 \text{ psi}$$

# Engineering Calculations – Rear 4

## Axle types [95]

Axle type	Pro	Con
Universal Joint (U-Joint)	<ul style="list-style-type: none"> <li>-Easy to replace</li> <li>-Allows angle change</li> </ul>	<ul style="list-style-type: none"> <li>-Acts as a suspension member</li> <li>-More stress on drivetrain's subsystems</li> <li>-Rougher ride</li> <li>-Spline- Very expensive to buy and can't manufacture at machine shop.</li> </ul>
Constant-Velocity axle (CV)	<ul style="list-style-type: none"> <li>-Allows angle change</li> <li>-Changes length at different points in travel (plunges)</li> <li>-Cheaper</li> </ul>	<ul style="list-style-type: none"> <li>-Hard to replace</li> </ul>

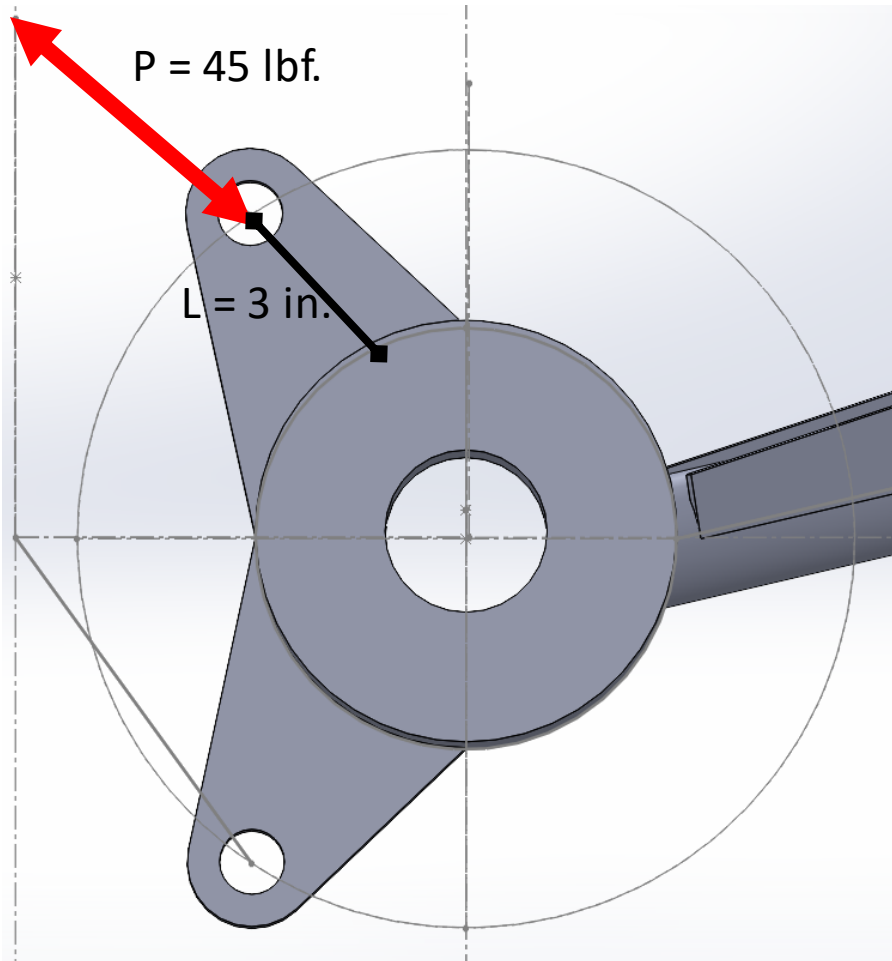
CV – Axle max/min length



Change in length needed for suspension geometry	Change in length of CV Axle	Change in U-joint (Non-spline)
1.5 in	1-3 in	0 in

# Engineering Calculations – Rear 5

## Knuckle Design [97]



$\sigma = \text{Normal Stress, psi}$

$\tau = \text{Shear Stress, psi}$

$P = \text{External Applied Load, lbf}$

$L = \text{Linear Distance, in}$

$h = \text{Size of Weld, in}$

$l = \text{length of Weld, in}$

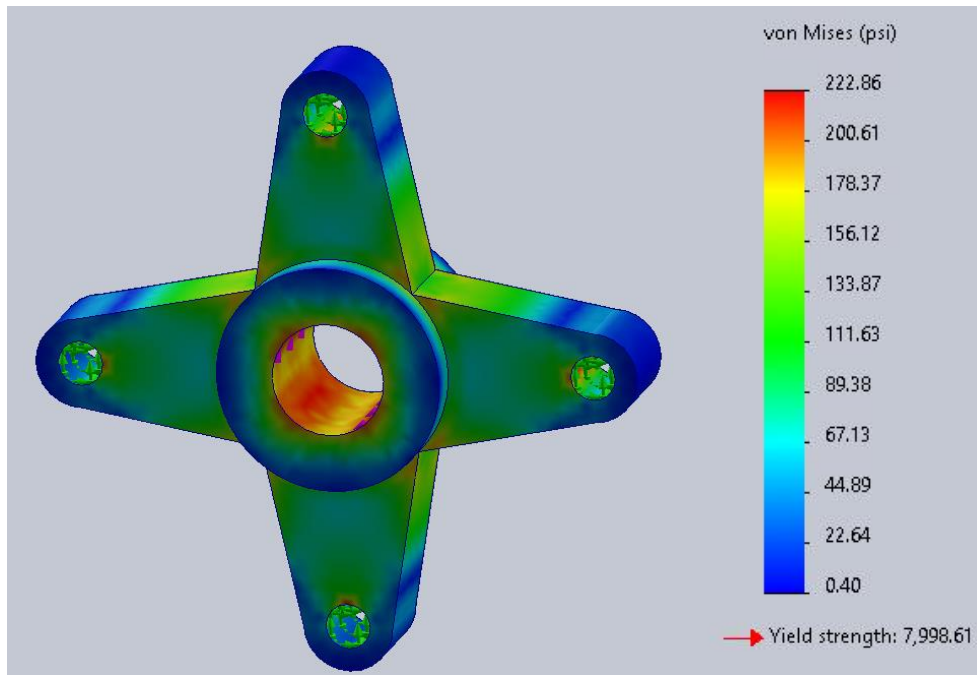
$$\sigma_b = \frac{6PL}{lh^2} = 1,270.59 \text{ psi}$$

$$\tau = \frac{P}{lh} = 35.29 \text{ psi}$$

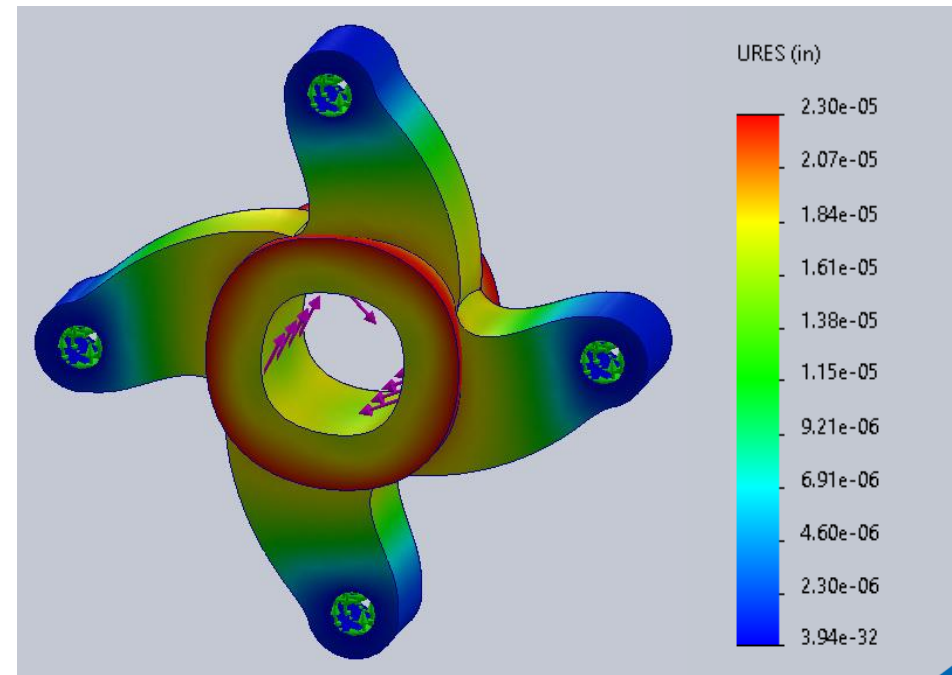
# Engineering Calculations – Rear 6

## Hub Design

### Stress Analysis



### Displacement Analysis



# Engineering Calculations – Rear 7 Hardware

## Black-Oxide Alloy Steel



- $S_{UT} = 90,000 \text{ psi}$
- Tensile = 170,000 psi
- Mass density =  $0.2782 \text{ lb/in}^3$
- Cheap!
- \$1.82 per screw
- Many size options

## 18-8 Stainless Steel



- $S_Y = 31,200 \text{ psi}$
- $S_{UT} = 73,200 \text{ psi}$
- $\rho = 0.2890 \text{ lb/in}^3$
- \$7.58 per screw
- Corrosion Resistant

## Grade 2 Titanium

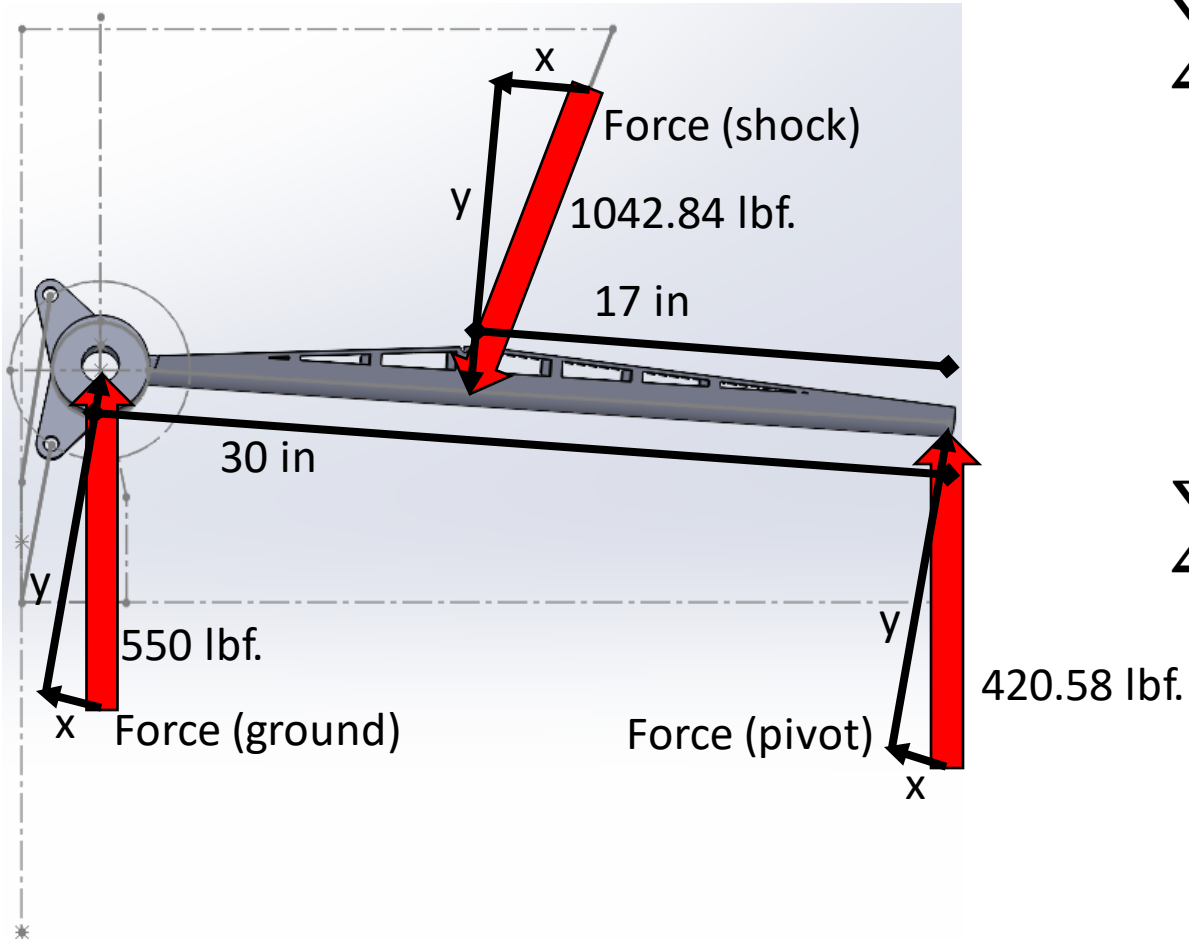


- $S_Y = 39,900 - 59,500 \text{ psi}$
- $S_{UT} = 49,900 \text{ psi}$
- 40% Lighter than Carbon Steel
- $\rho = 0.1629 \text{ lb/in}^3$
- Expensive!
- \$54.54 per screw



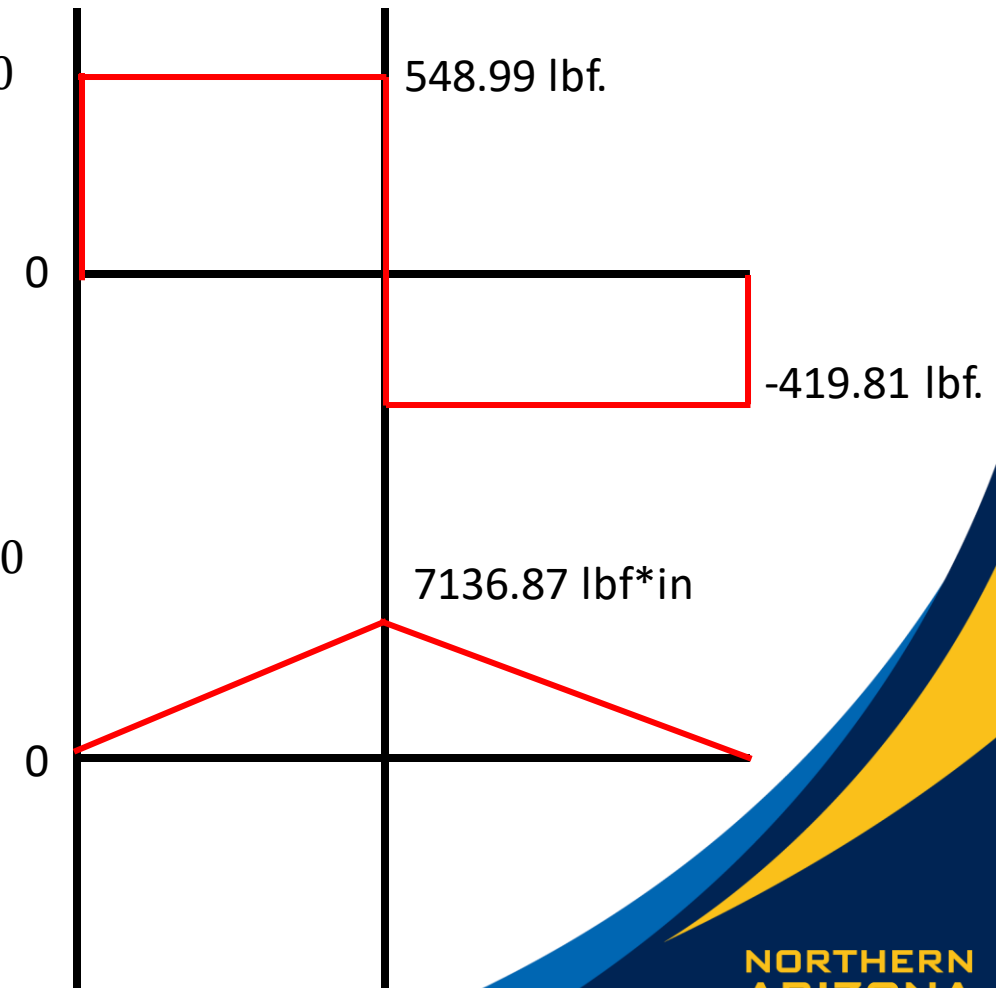
# Engineering Calculations – Rear 8

## Trailing Link Design



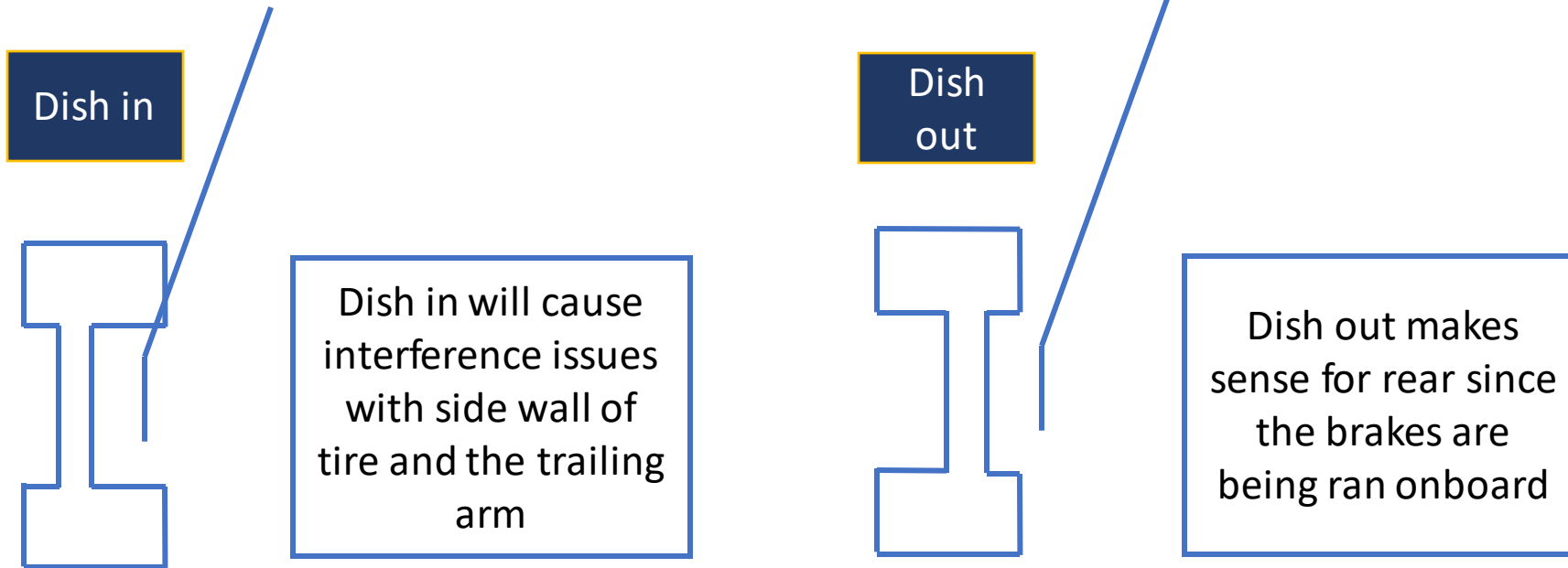
$$\sum F = 0$$

$$\sum M = 0$$



# Engineering Calculations – Rear 9

## Wheel Dish Design



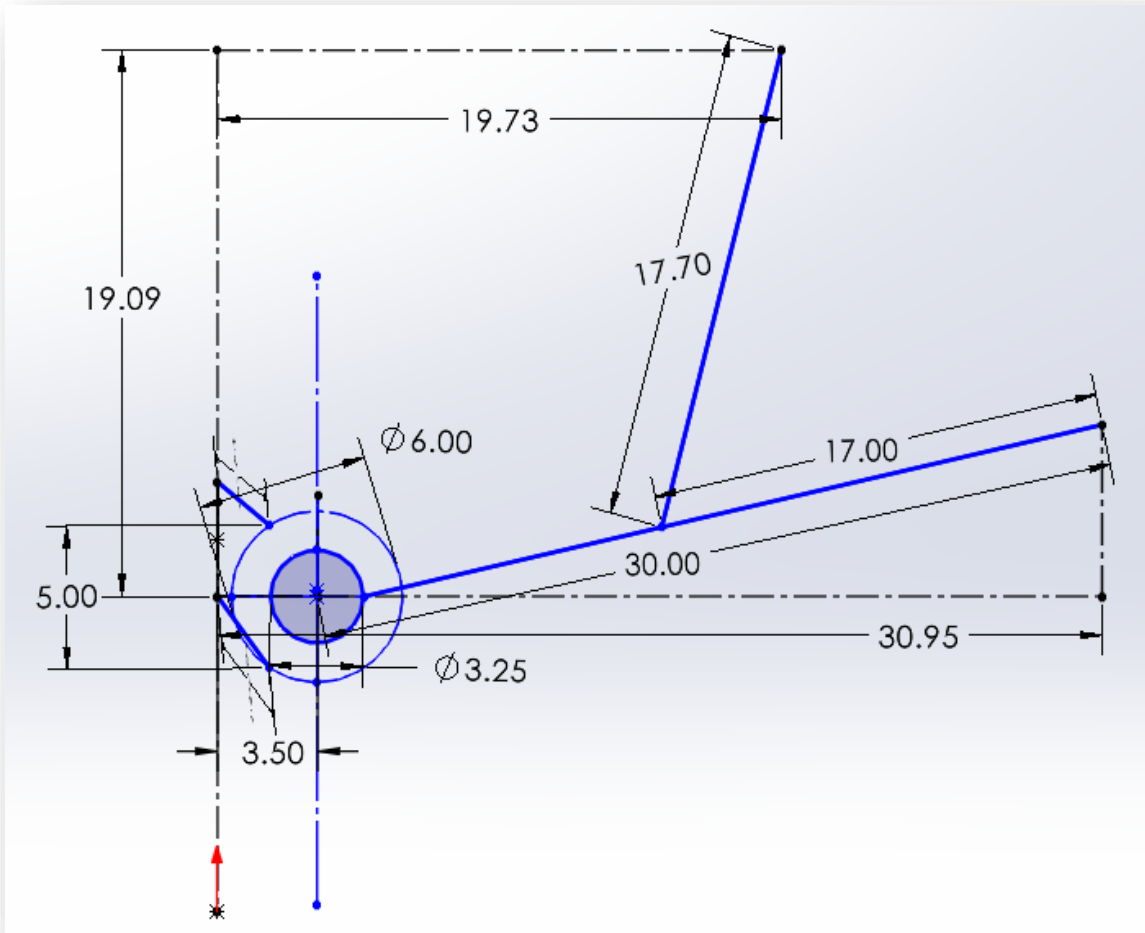
# Concept Evaluation

Subsystem	Variants					
	1	Results	2	Results	3	Results
Camber	Positive	✓	Negative	✓	Neutral	✓
Toe	In	✗	Out	✗	Neutral	✓
Camber Link Material	Carbon Fiber	✗	Steel	✓	Alumminium	✓
Axle types	CV Axle	✓	Dogbone	✗	U-Joint axle	✗
Knuckle Design	CNC Machined Aluminum	✗	Steel	✓	Attach knuckle to trailing arm	✓
Hub	Aluminum (machined)	✓	Cast	✗	NA	
Hardware	Stainless Steel	✗	Steel	✓	Titanium	✗
Trailing Link Design	Boxed Sheet Metal	✓	Steel Tubing	✓	CNC Machined Aluminum	✗
Wheel dish	Dish out	✓	Dish in	✗	NA	

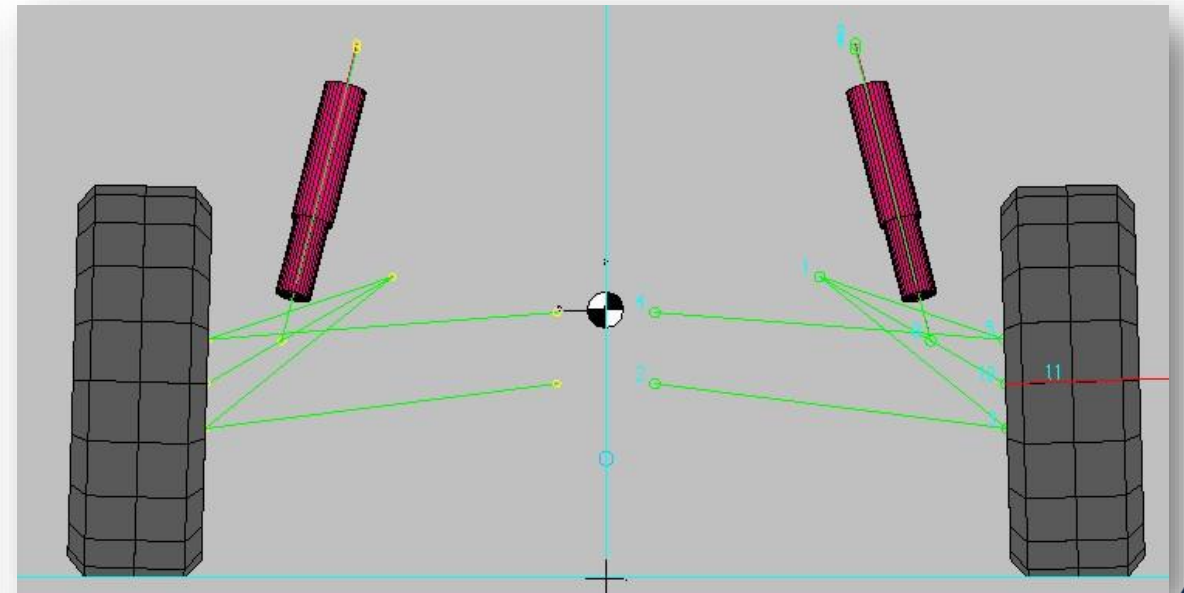
# Concept Evaluation

Subsystem	Variants					
	1	Results	2	Results	3	Results
Camber	Positive	✓	Negative	✓	Neutral	✓
Toe	In	✗	Out	✗	Neutral	✓
Camber Link Material	Carbon Fiber	✗	Steel	✓	Alumminium	✓
Axle types	CV Axle	✓	Dogbone	✗	U-Joint axle	✗
Knuckle Design	CNC Machined Aluminum	✗	Steel	✓	Attach knuckle to trailing arm	✓
Hub	Aluminum (machined)	✓	Cast	✗	NA	
Hardware	Stainless Steel	✗	Steel	✓	Titanium	✗
Trailing Link Design	Boxed Sheet Metal	✓	Steel Tubing	✓	CNC Machined Aluminum	✗
Wheel dish	Dish out	✓	Dish in	✗	NA	

# Final Design Discussion

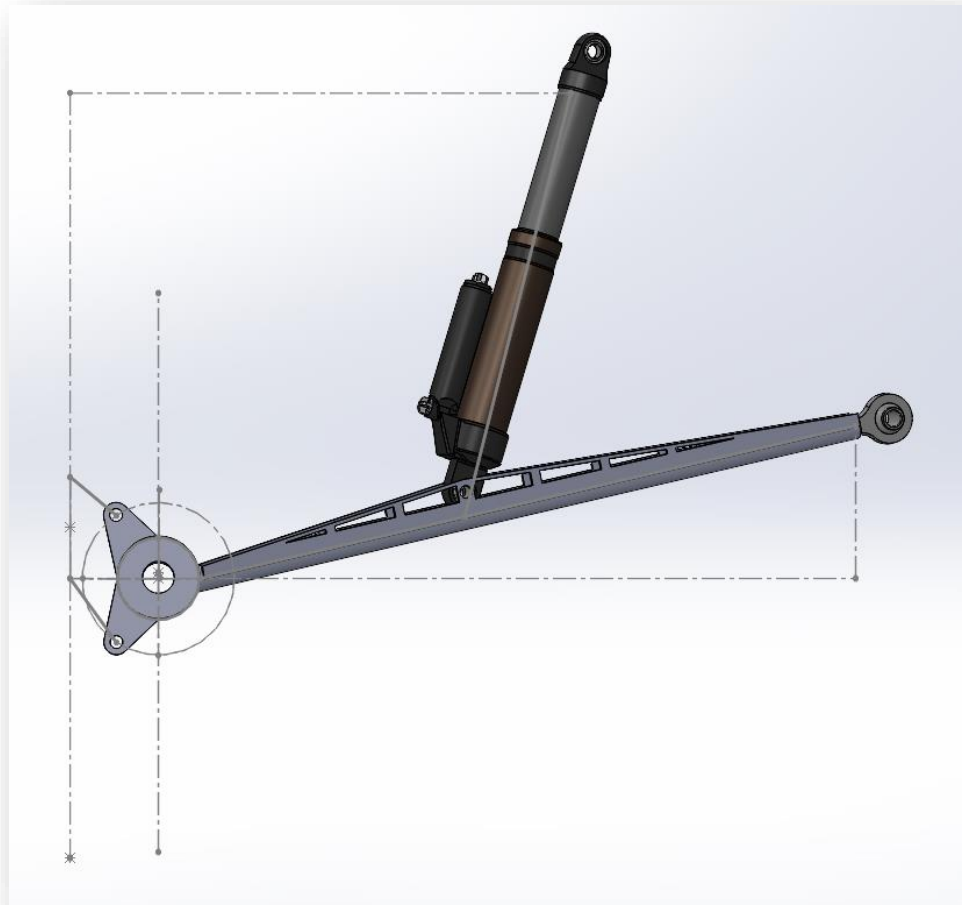


Right view wire frame dimensions

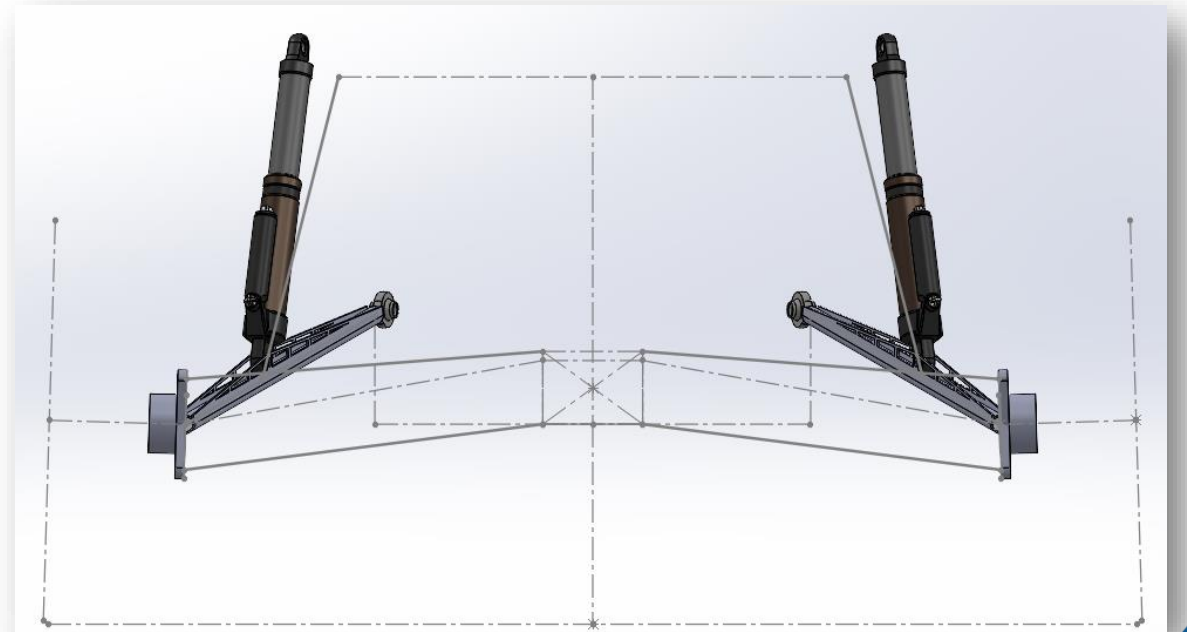


Rear view suspension geometry in Shark

# Final Design Discussion



Right view of trailing link assembly



Rear view of trailing link assembly

# Bill of Materials – Rear

Suspension	Quantity	Cost	Drive	Quantity2	Cost2	Overall Total:
Trailing link	2	\$70.00	CV axles	2	\$110.00	
Camber link	4	\$50.00	Knuckles	2	\$120.00	
Shocks	2	\$0.00	CV bearings	2	\$0.00	
Rod ends	10	\$80.00	Hubs	2	\$400.00	
Pivot hardware	28	\$50.00	Wheels	2	\$0.00	
Frame mounts	8	\$30.00	Tires	2	\$0.00	
PVC	1	\$10.00	Wheel nuts	8	\$20.00	
Spares	4	\$120.00	CV hardware	2	\$0.00	
			Spares	3	\$200.00	
<b>Total:</b>	59	<b>\$410.00</b>	<b>Total:</b>	25	<b>\$850.00</b>	<b>\$1,260.00</b>

# Rear End Budget

	Category	Relevant Items	Approximated Cost
1	Vehicle Expenses	Suspension System Drive System  <b>Estimated Total</b>	\$410 \$850  <b>\$1,260</b>
2	Spare Parts	Camber links, rod ends, cv axles, hubs	\$320
3	Competition Expenses Rear Sub-team	Registration, travel (hotel rooms, vehicle rentals, gas, etc.)	\$1,125
4	Contingency (5%)	Unpredicted Expenses	\$135
		<b>Total</b>	<b>\$2,840</b>



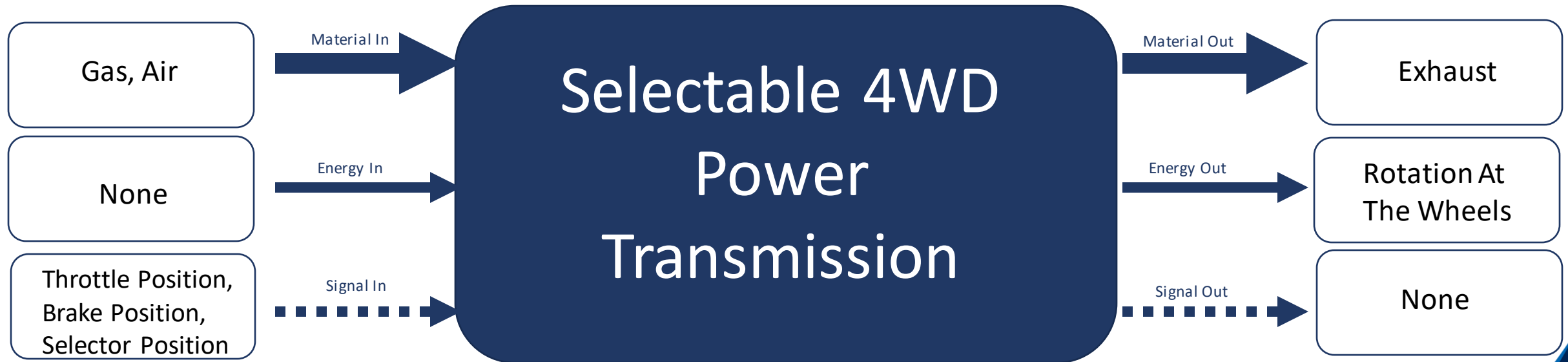
**NAU**

# Drivetrain Team

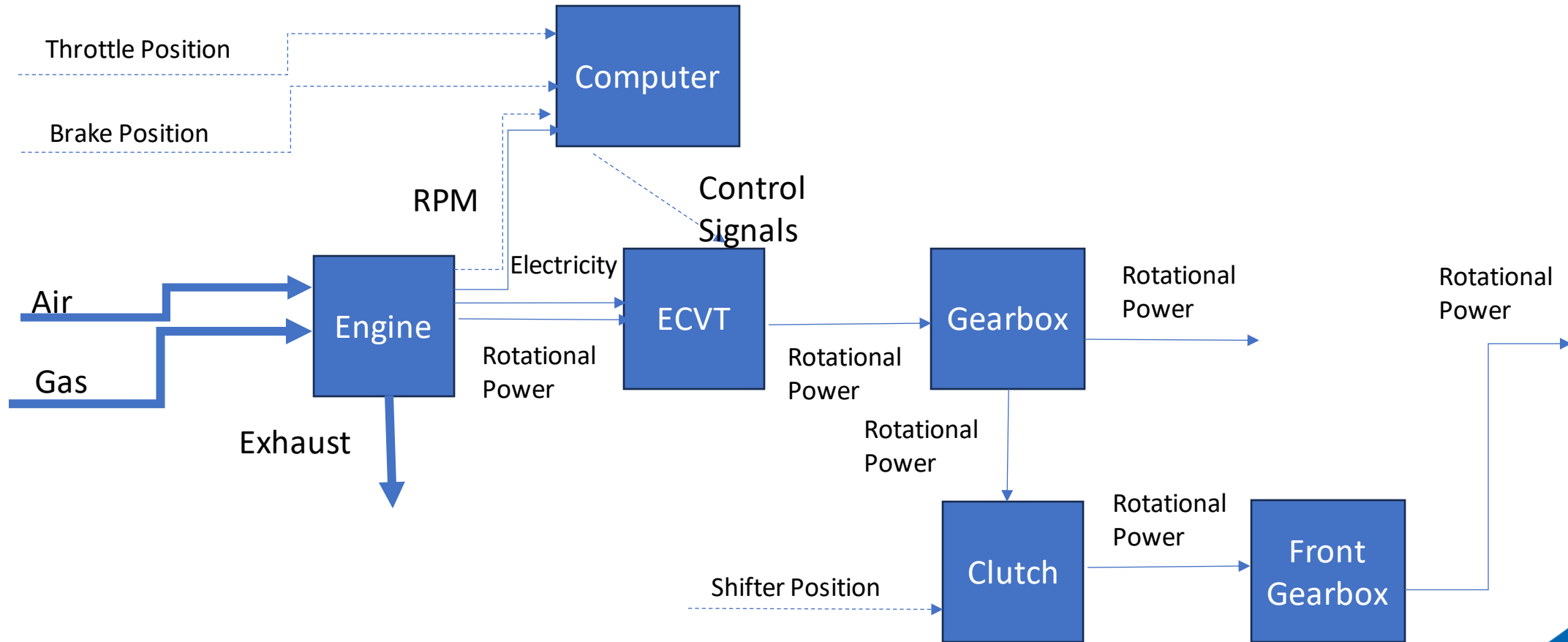
Henry Van Zuyle, Donovan Parker, Ryan  
Fitzpatrick, Jarett Berger

**NORTHERN  
ARIZONA**  
UNIVERSITY

# Black Box Model - Drivetrain



# Functional Model - Drivetrain



# Concept Generation - Drivetrain

Concept Generation Subsystem	Variants		
	1	2	3
CV Joint Integration			
Dog Clutch Choice			
Rear Brake Integration			
CVT System Choice			

## Sub-System Influence

Compact Front End and Reduce Weight

Selectable 4-Wheel Drive

Optimize Rear End Geometry  
Reduce Weight

Change Gears and Allow a High Total Ratio

# Engineering Calculations – Drivetrain 1

## Equations, Tools, & Examples

Equations:

- $\Delta r = r_o - r_i$ ,  $\Delta d = 2 \times \Delta r$
- $F = \frac{T}{r_i/12} = 1742.0 \text{ lbs}$
- $\sigma = \frac{F}{A} = 11,531 \frac{\text{lb}}{\text{in}^2}$
- $n = \frac{\pi S \Delta d^2}{4F} = 28.84$
- $a = \frac{F}{m} = 553.35 \frac{\text{ft}}{\text{s}^2}$

Where:

T = Torque

F = Force

$\sigma$  = Normal Stress on Teeth

A = Planar Surface Area on Teeth

a = Acceleration

r = Radius, d = Diameter

m = mass

S = Material Strength

n = Factor of Safety

Analysis Tool: MATLAB

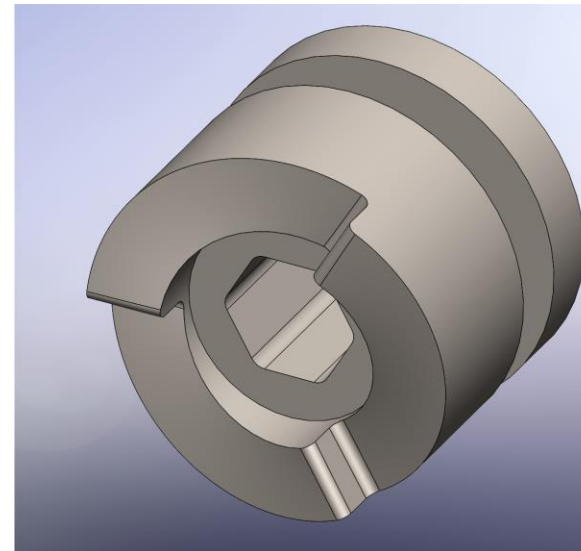
```

clc; clear; close all;
% All units are IPS
% Material: 4130 Steel Annealed at 865C (Non Heat Treated)
%Knowns
%{
Torque, Material Strength, Outer Radius, Inner Radius, Tooth Surface
Area, Mass
%}
T=126.66; S=81221.13; r_o=1.5; r_i=0.872516; A=0.151073; m=3.148067;
%Calculations
% Radius Difference
dr=r_o-r_i; % inches
% Force
F=T/(r_i/12); %pounds
% Normal Stress on teeth on contact
sigma_t=F/A; %psi
% Factor of Safety
n=((pi*S*(2*dr^2))/(4*F)); %unitless
% Engage Acceleration
a=F/m; %ft/sec^2
    
```

Spiral Jaw Dog Clutch

- Forces
- Tooth Normal Stress
- Factor of Safety
- Acceleration

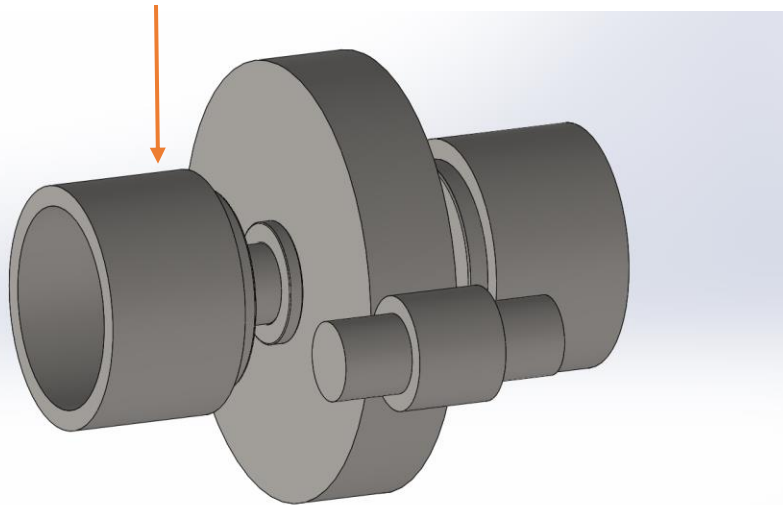
Modeling  
Material:  
4130 Steel  
Annealed at  
865C



# Engineering Calculations – Drivetrain 2

## CV Joint Integration

### Radial Load



### Analysis

```

H = 11.45; % Horsepower (HP)
N = 3600; % Desired speed (rev/min)
G1 = 17; % Number of teeth
G2 = 65; % Number of teeth
D = 12; % Diametral Pitch (teeth/in)
p = 20; % Pressure Angle
DP1 = G1/D; % Diametral Pitch for Gear 1
DP2 = G2/D; % Diametral Pitch for Gear 2
Ti = (550*H*60)/(N*pi)*12; % Input Torque (lb*in)

Rx = Ti/(DP2/2); % Reaction force in x direction
Ry = Rx*tan(p); % Reaction force in y direction
R = sqrt(Rx^2+Ry^2); % Resultant Bearing Reaction Force
disp(R) % Displays Bearing Reaction Force

Fr = 39.3822; % Bearing Reaction Force
a = 1/3; % Bearing load life
LD = 1000; % Desired design life (hours)
LR = 10^6; % Rating life (hours)

L = LD*N*60; % Desing life
C = Fr/(LR^a); % Catalog Load Rating Equation
disp(C) % Displays Catalog Load Rating
    
```

### Results

Sprag nominal torque = **75lbf**

Bearing reaction force = **39.7lb**

Catalog load rating = **8506.56lbf** or **37.8kN**

### Equations

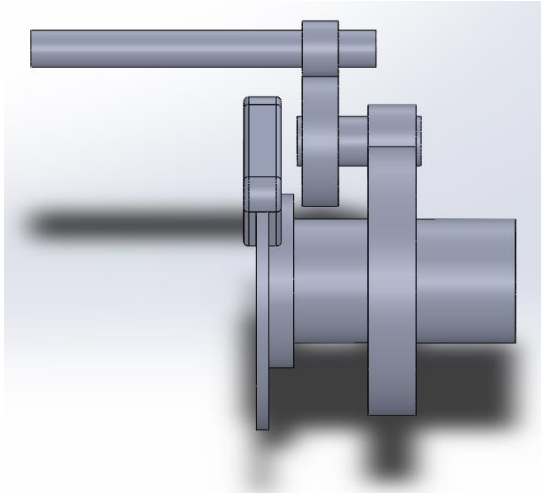
$$F_D (\mathcal{L}_D n_D 60)^{1/a}$$

$\mathcal{L}_D$  — desired life, hours  
 $n_D$  — desired speed, rev/min  
 $F_D$  — desired radial load, lbf or kN

$$C_{10} = F_R = F_D \left( \frac{L_D}{L_R} \right)^{1/a} = F_D \left( \frac{\mathcal{L}_D n_D 60}{\mathcal{L}_R n_R 60} \right)^{1/a}$$

# Engineering Calculations – Drivetrain 3

## Equations, Tools, & Examples



Option 2 : Optimal Gearbox Geometry

```
d_gearbox = gear5_pitch_diameter ; % Depth of gearbox casing at point of
interest (in)
t_gearbox = 0.125 ; % Thickness of gearbox casing
L_reduction = (0.5*gear4_pitch_diameter + gear5_pitch_diameter) -
(0.5*gear3_pitch_diameter) ; % Length of casing material reduction (in)
w_reduction = gear_width_23 + 0.1 ; % Width of casing material reduction (in)
V_reduction =
(2*(L_reduction*w_reduction*t_gearbox))+(w_reduction*d_gearbox*t_gearbox) ; %
Volume of reduced material (in^3)
density_Al = 0.0975 ; % Density of 6061 T6 Aluminum (lb/in^3)
Weight_reduction_lbs = V_reduction*density_Al % Weight of gearbox casing
removed (lbs)
density_St = 0.284 ; % Density of 4140 Steel (lb/in^3)
Weight_shaftA_increase_lbs = (1.0667*((pi/4)*0.75^2))*density_St % Weight of
Shaft A material increase (lbs)
Weight_Frontshaft_increase_lbs = (1.0667*((pi/4)*1^2))*density_St % Weight of
Front Shaft material increase (lbs)
net_Weight_reduction_lbs = Weight_reduction_lbs - Weight_shaftA_increase_lbs -
Weight_Frontshaft_increase_lbs % Net weight reduction of Option 3 compared to
Option 2.
```

```
Weight_reduction_lbs =
```

```
0.1512
```

```
Weight_shaftA_increase_lbs =
```

```
0.1338
```

```
Weight_Frontshaft_increase_lbs =
```

```
0.2379
```

```
net_Weight_reduction_lbs =
```

```
-0.2205
```

### MATLAB Script for Calculations

### Results of Calculations:

Net Weight Reduction of Option 3 = -0.2205 lbs  
This means that Option 3 (flipping stage 1 to passenger side of vehicle) results in a weight GAIN of 0.2205 pounds. Option 2 eliminates the brake caliper interference from Option 1 and weighs less than Option 3 with less design alterations than Option 3.

### Equations:

$$Weight = V_{component} * \rho_{material}$$

$$\text{Where... } V = Volume (in^3)$$

$$\rho = density \left( \frac{lb}{in^3} \right)$$

$$\rho_{steel,4140} = 0.285 \frac{lb}{in^3}$$

$$\rho_{aluminium,6061 T6} = 0.0975 \frac{lb}{in^3}$$

# Engineering Calculations – Drivetrain 4 ECVT Motor Specs

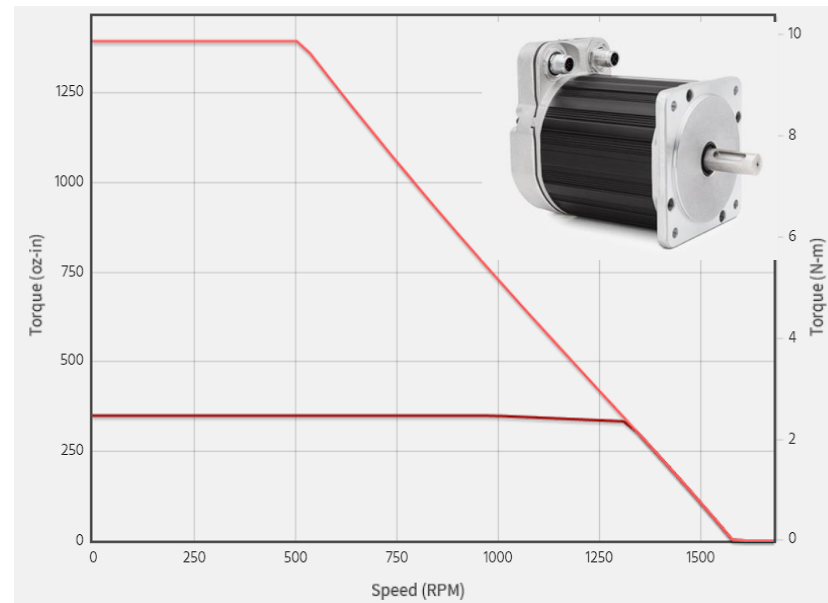
$$T_R = \frac{Fd_m}{2} \left( \frac{l + \pi f d_m}{\pi d_m - fl} \right)$$

- Force = 429.7 Lbf
- ½-10 lead screw
- Coef. Friction = .2

Max torque required from motor is 448 oz in

These equations calculate what torque output the ECVT Control motor needs to generate.




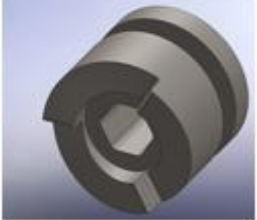
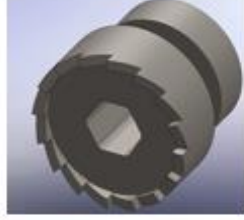
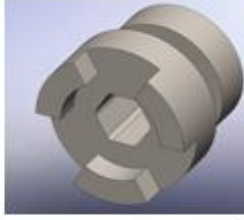

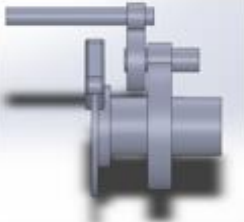
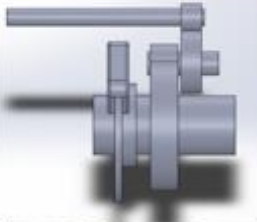
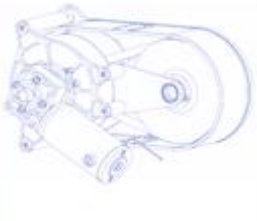


Hudson M-3432F-LS-08D





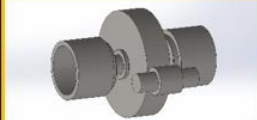
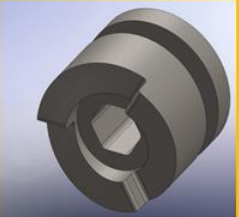
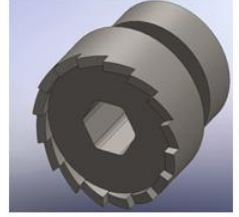
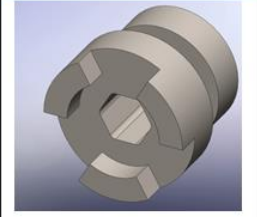
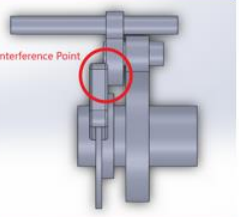
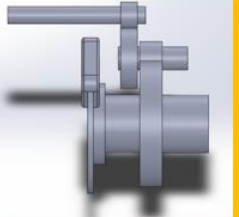
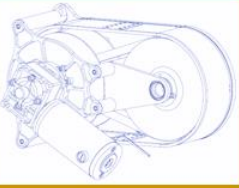
- $P=IV$
- $I = 12A$
- $V = 48V$
- Max motor power is 576 watts



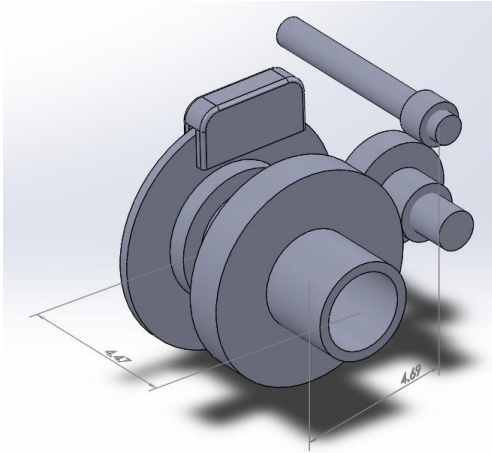
# Concept Evaluation - Drivetrain

Concept Evaluation Subsystem	Variants					
	1	Rating	2	Rating	3	Rating
CV Joint Integration		X		X		✓
Dog Clutch Choice		✓		X		X
Rear Brake Integration		X		✓		X
CVT System Choice		✓		X		X

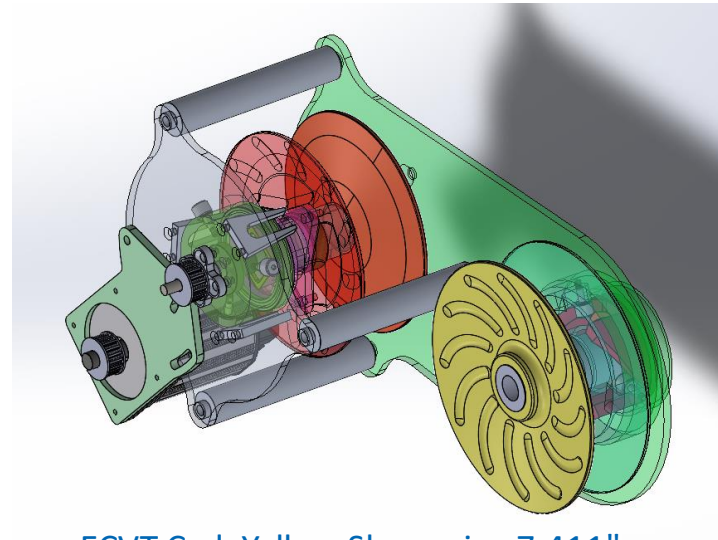
# Final Design Discussion - Drivetrain

Concept Evaluation Subsystem	Variants					
	1	Rating	2	Rating	3	Rating
CV Joint Integration		✗		✗		✓
Dog Clutch Choice		✓		✗		✗
Rear Brake Integration		✗		✓		✗
CVT System Choice		✓		✗		✗

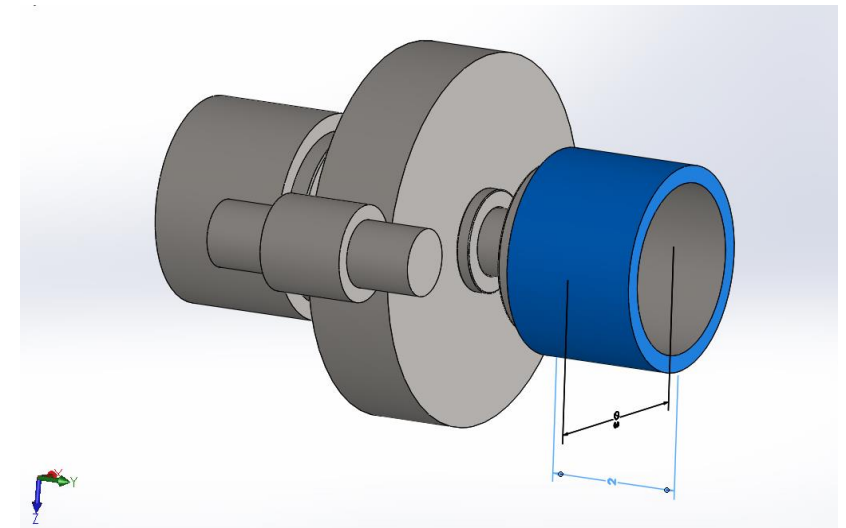
# Final Design Visualization - Drivetrain



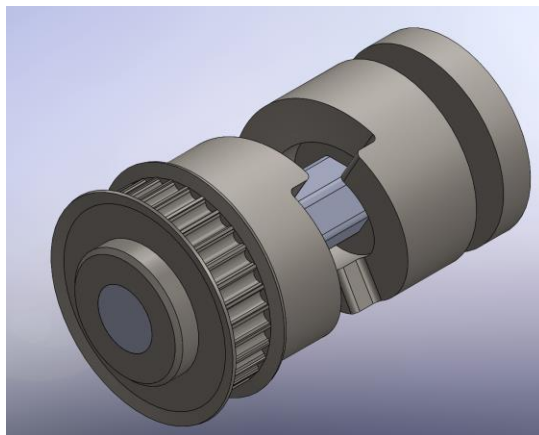
Rear Gearbox CAD, Approximate  
Dimensions Are: 6"x8"x4.5"



ECVT Cad, Yellow Sheave is  $\varnothing 7.411$ "



Front Gearbox CAD, CV Cup Width is 2"



Four-Wheel Drive Integration, 3"  
Diameter Belt Pulley

# Bill of Materials – Drivetrain

Clutch System				ECVT				ECVT				Summary	
Part	Quantity	Cost (\$)	Total \$	Part	Quantity	Cost \$	Total \$	Part	Quantity	Cost \$	Total \$	Sub-System	Total (\$)
Driven Side Clutch	1	59.00	59.00	ECVT Primary Shaft	1	25.00	25	ECVT Secondary Moving Sheave	1	75	75.00	Clutch System	1336.57
Driving Side Clutch	1	59.00	59.00	ECVT Primary Fixed Sheave	1	70.00	70	ECVT Secondary Cam	1	50	50.00	ECVT	3210.00
Shift Fork	1	21.49	21.49	ECVT Primary Mobile Sheave	1	70.00	70	ECVT Secondary Cam Nut	1	15	15.00	Front Gearbox	794.00
High Strength HTD Timing Belt	2	99.00	198.00	ECVT Primary Square Bushing	1	25.00	25	ECVT Backplate	1	60	60.00	Rear Gearbox	1018.55
3in Belt Pulley	1	5.35	5.35	ECVT Primary Sliding Shaft	1	40.00	40	ECVT Main Mounting Plate	1	30	30.00		
4.5in Belt Pulley	1	10.92	10.92	ECVT Primary Lead Screw Flange	1	50.00	50	ECVT Main Mount Standoff	3	20	60.00		
Idler Pulleys	11	52.25	574.75	ECVT Primary Lead Screw nut	1	75.00	75	ECVT Lead Screw Bearing Mount	1	4	4.00		
Housing	1	25.43	25.43	ECVT Primary Lead Screw	1	25.00	25	ECVT Motor Mount PLate	1	15	15.00		
Shifter	1	32.99	32.99	ECVT Primary Mobile Sheave Bushing	1	10.00	10	ECVT Controll Pulley	2	5	10.00		
Linkage Cables	1	78.74	78.74	ECVT Secondary Shaft	1	50.00	50	ECVT Lead Screw Nut Flange Fork	3	2	6.00		
Cable Tabs	10	27.09	270.90	ECVT secondary Fixed Sheave	1	75.00	75	Engine	1	900	900.00		
Front Gearbox				Rear Gearbox				ECVT					
Part	Quantity	Cost (\$)	Total \$	Part	Quantity	Cost \$	Total \$	Part	Quantity	Cost \$	Total \$		
Bearings, SKF 210-ZNR	4	80	320	Bearings, SKF 210-ZNR	2	80	160	Control Motor	1	500.00	500		
Sprag, GMN FK6205-2RS	2	80	160	Bearings, 6206	2	35	70	Control Motor Cables	2	90.00	180		
Circlips	2	2	4	Bearings, 6208	1	80	80	Arduino	1	70.00	70		
Gear 1	1	30	30	Bearings, 6212	1	175	175	Motor Controller	1	220.00	220		
Gear 2	1	50	50	Gears 2-4	1	74.56	74.56	Boost converter	1	60.00	60		
Housing	2	75	150	Gear 5	1	290	290	Buck Converters	2	10.00	20		
Shaft	2	30	60	Gearbox Casing (6061 Aluminum)	1	108.99	108.99	Sensors	1	50.00	50		
Hardware	1	20	20	Shaft (4140 Steel)	2	30	60	Hardware	1	20.00	20		
								Bearings	1	170.00	170		
								Belts	2	90.00	180		

# Drivetrain Budget

	Category	Relevant Items	Approximated Cost
1	Vehicle Expenses	Motor Front Gearbox Rear Gearbox ECVT 4WD  <b>Estimated Total</b>	\$900 \$794 \$1018.55 \$2310 \$1336.57  <b>\$6359.12</b>
2	Spare Parts	Hardware, Gears, CV axles	\$500
3	Competition Expenses Drivetrain Sub-team	Registration, travel (hotel rooms, vehicle rentals, gas, etc.)	\$1,125
4	Contingency (5%)	Unpredicted Expenses	\$300
		<b>Total</b>	<b>\$8284.12</b>

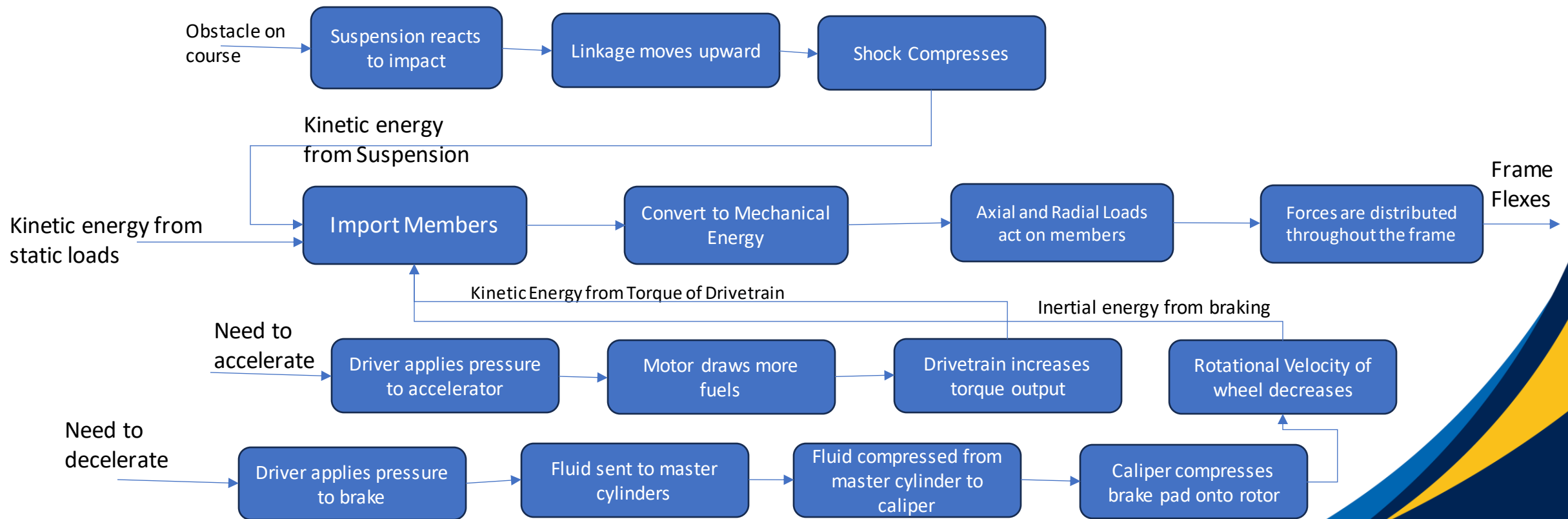
# Frame Team

Cooper Williams, Gabriel Rabanal, Antonio Sagaral

# Black Box Model



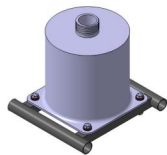
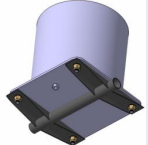

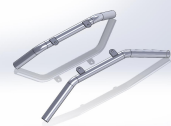
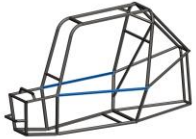



# Functional Model





# Concept Generation

Subsystem	Variant 1	Variant 2
Frame Type		
Fuel Tank Mounting		
Seat Design		
Side Impact Member		
Tube Material	AISI 4130	AISI 1018

# Engineering Calculations – SIM

## Equations, Tools, & Examples

### Flared SIM's

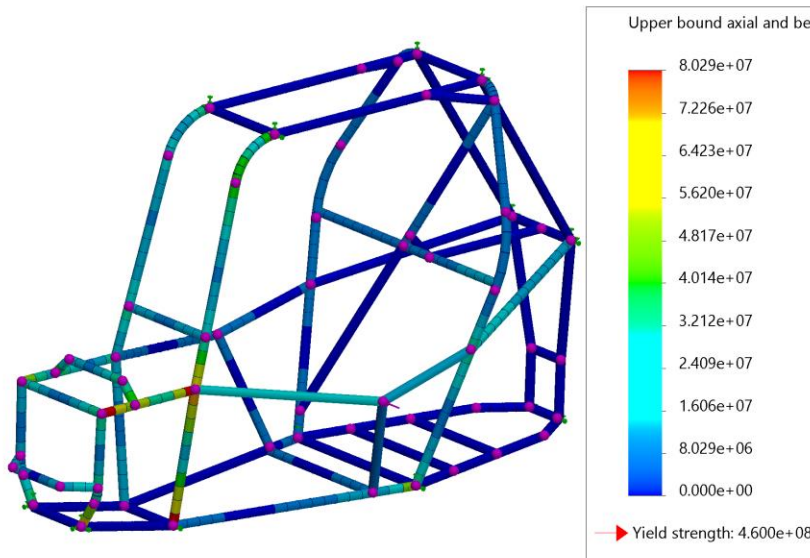
- Fewer members in parallel
- Overall vehicle length shortened
- Lower Egress time

Engineering Recs	Variants	
	Flared SIM	Straight SIM
Maximum Width (in)	32	28
Total Primary Tubing (ft)	45	48
Total Secondary Tubing (ft)	45	49
Overall Vehicle Length (in)	67	75

Governing Equations:

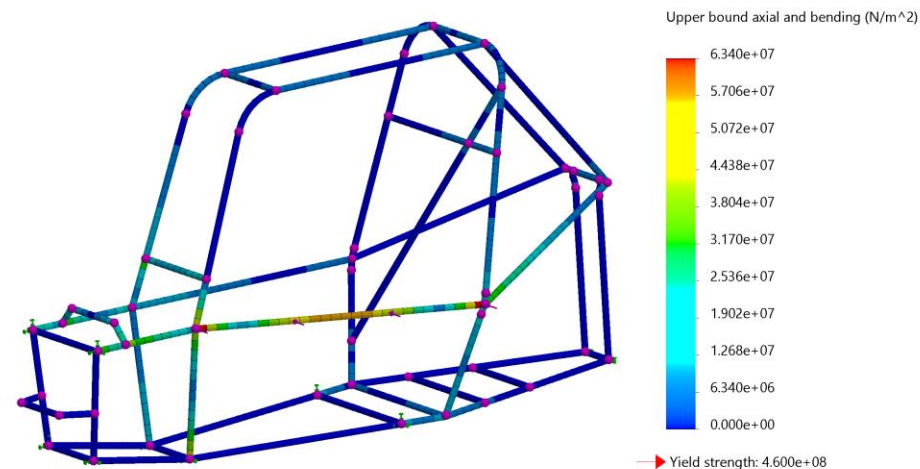
$$I = \frac{\pi}{4} (R^4 - R_i^4)$$

$$P = \frac{F}{A}$$



Flared SIM

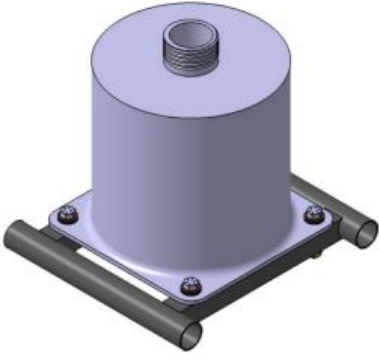
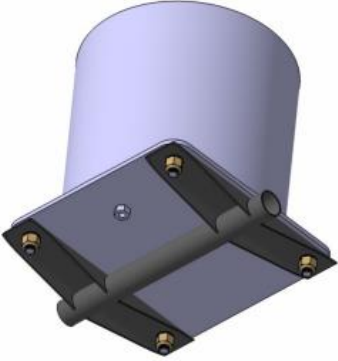
VS.



Straight SIM

# Engineering Calculations

## Equations, Tools, & Examples

	Variants	
Engineering Recs	Rectangular Tubing	C-Brackets
Figure		
Material Volume (in <sup>3</sup> )	6.9492	6.289
Weight (lb)	1.97357	1.78608
# of Weld Jigs	2-3	1-2
Types of alternative materials	1	0

$$Volume = (\pi r_o^2 - \pi r_i^2) * L$$

\*Rectangular tubing substituted for circular tubing for simplicity\*

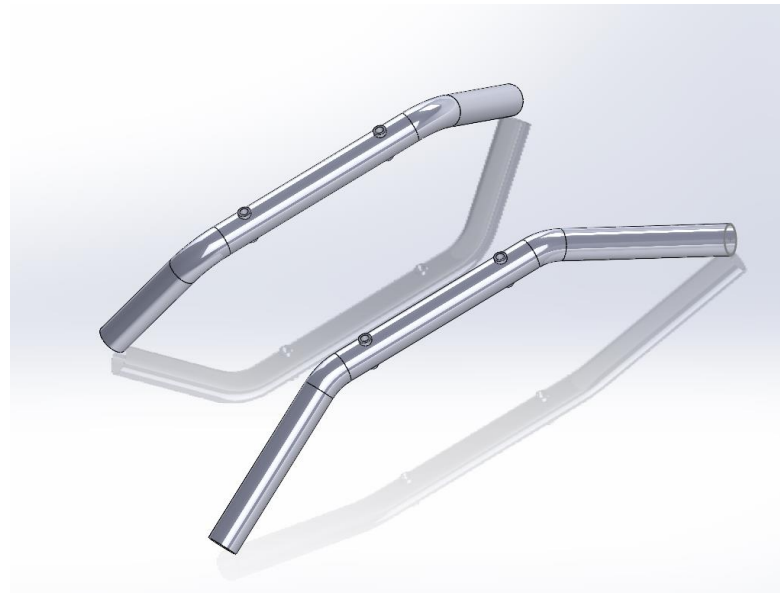
\*C-Bracket volume calculated using Solidworks tools\*

$$Weight = \frac{\rho}{V}$$

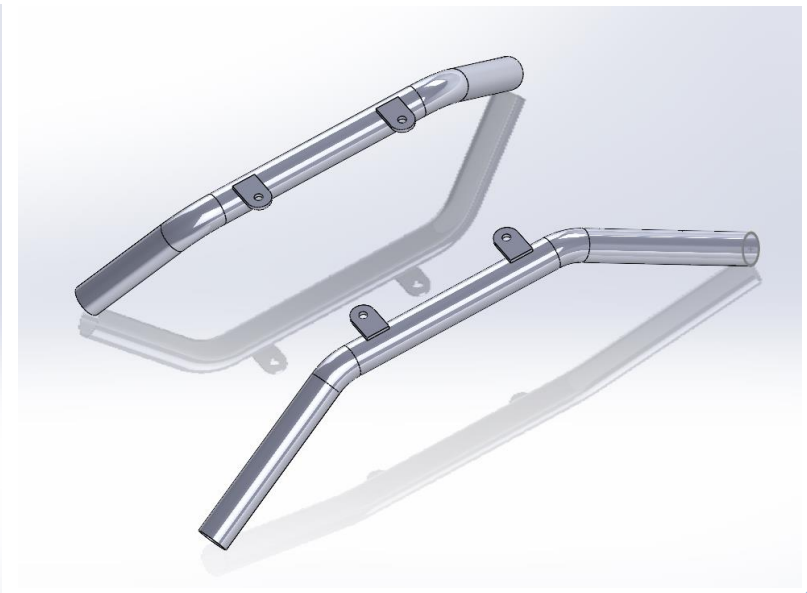
# Engineering Calculations – Lower Seat Mount

## Equations, Tools, & Examples

Variant 1



Variant 2



	Variant 1	Variant 2
Total Material volume (in <sup>3</sup> )	4.27	4.35
Ease of manufacturing	+	-

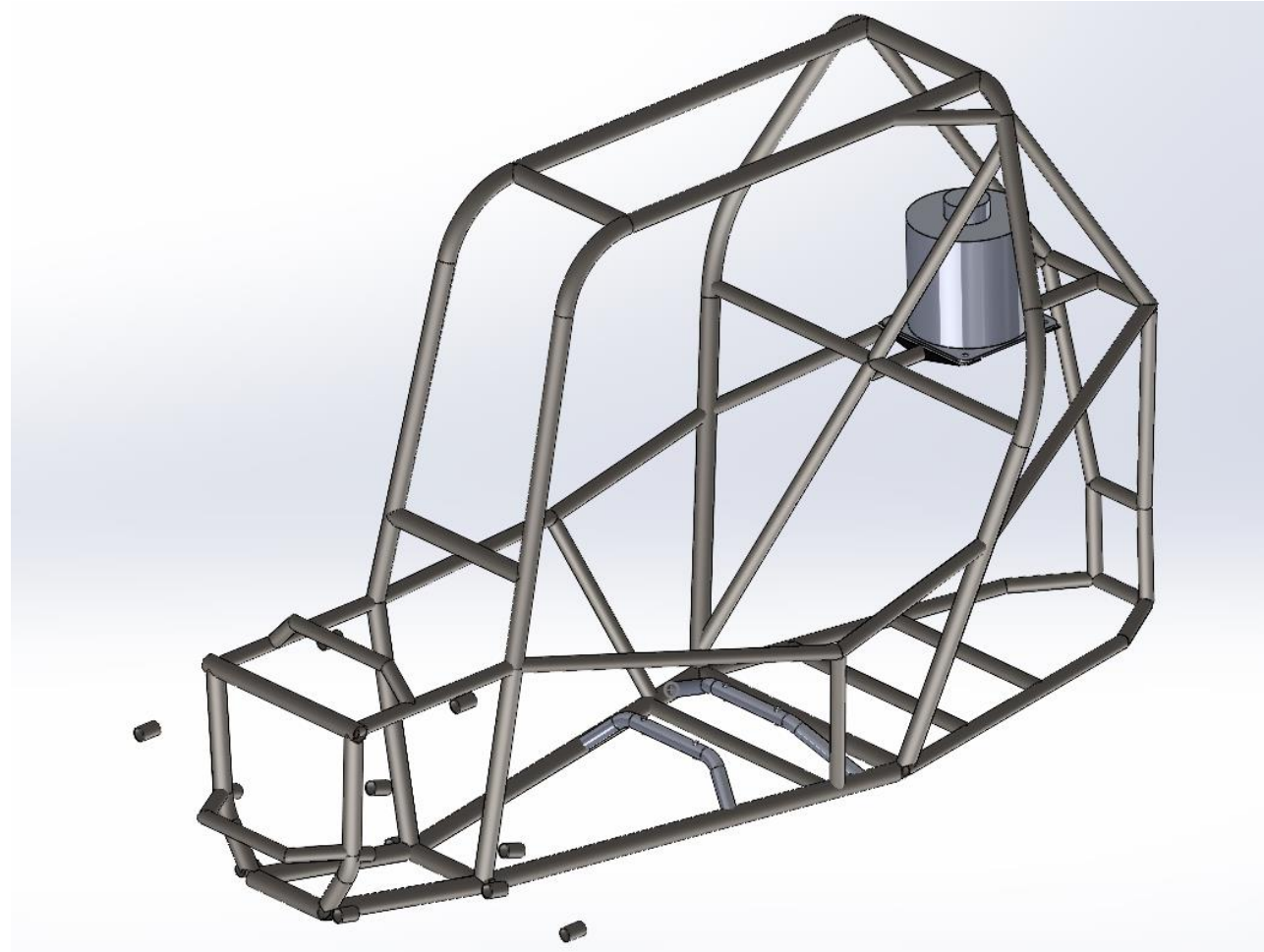
# Concept Evaluation

Subsystem	Variants			
	1	Rating	2	Rating
<i>Frame Type</i>	Front Brace	X	Rear Brace	✓
<i>Fuel Tank Mount</i>	Square Brackets	X	C-Brackets	✓
<i>Seat Design</i>	Slotts	✓	Tabs	X
<i>Side Impact Members</i>	Straight	X	Flared	✓
<i>Tube Material</i>	AISI 4130	✓	AISI 1018	X

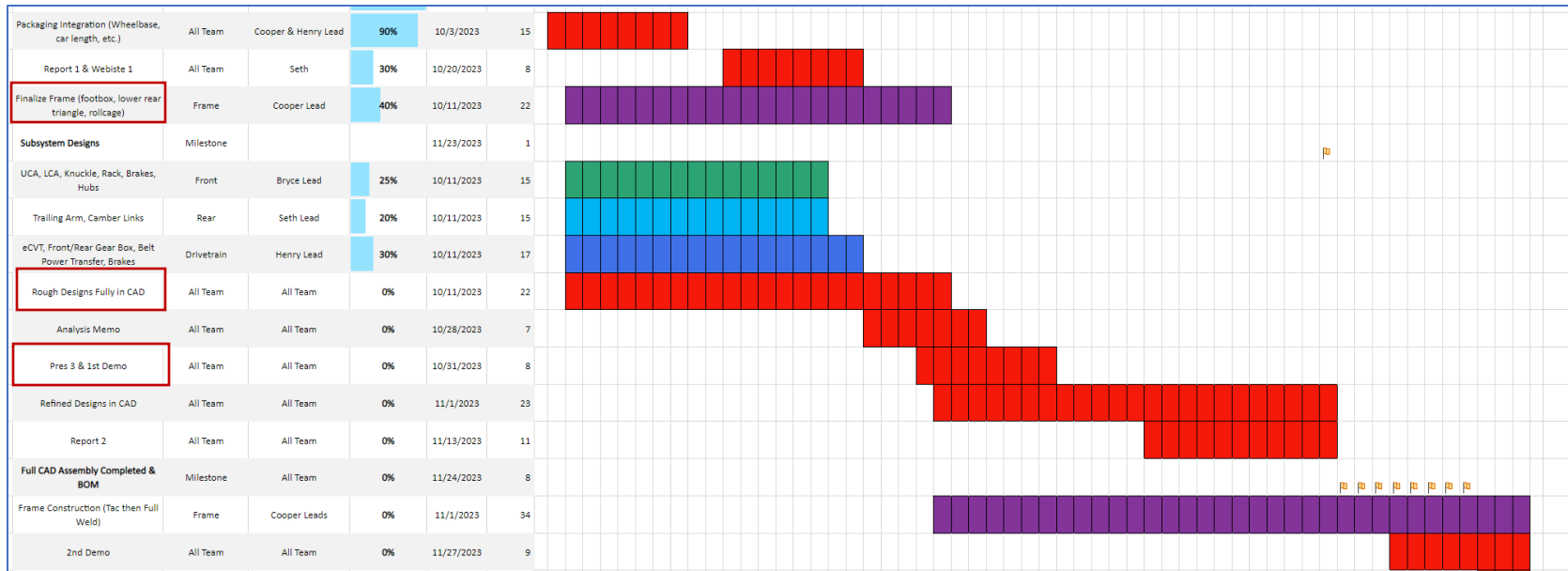
# Final Design Discussion

Subsystem	Variants			
	1	Rating	2	Rating
Frame Type	Front Brace	X	Rear Brace	✓
Fuel Tank Mount	Square Brackets	X	C-Brackets	✓
Seat Design	Slots	✓	Tabs	X
Side Impact Members	Straight	X	Flared	✓
Tube Material	AISI 4130	✓	AISI 1018	X

# Final Design Visualization



# Project Schedule



**Frame**

Purchase

Material

10/13/2023

Complete

Integration

10/27/2023

Prototype

11/10/2023



# Bill of Materials

SAE Baja Frame						
Part	Description	Qty	Units	Unit Cost	Cost	Obtained
Primary Members	4130 1.25x.065" tubing	45	ft	7.00	315.00	N
Secondary Members	4130 1x.035" tubing	45	ft	6.00	270.00	N
Tabs	4130 0.1" sheet	100	in^2	0.28	27.78	N
Side Panneling	Carbon Weave	20	ft^2	6.00	120.00	N
Seat	Carbon Weave	4	ft^2	6.00	24.00	N
Epoxy	Carbon resin epoxy	1	gallon	85.00	85.00	N
Harness	Standardized	1	unit	100.00	100.00	Y
Submarine Straps	Standardized	2	unit	23.00	46.00	N
Fire Extinguisher	5BC Standard	1	unit	25.00	25.00	Y
Extinguisher Mount Bracket	Drake FIREX-MNT-DAG	1	unit	75.00	75.00	Y
Fuel Tank Mounting Washers	McMaster Carr 94733A723	8	50	14.00	2.24	Y
Mounting Hardware	Misc. nuts, bolts, washers needed	1	unit	50.00	50.00	N
Skid Plate	.06" HDPE	6	ft^2	5.00	30.00	N
Firewall	.02" sheet metal	9.5	ft^2	7.75	73.63	N
<b>Total Costs</b>					<b>1243.64</b>	<b>1041.40</b>

**Frame Team Materials Cost: \$1041**

\*Does not include materials sponsor discounts\*

# Frame Budget

	Category	Relevant Items	Approximated Cost
1	Vehicle Expenses	Frame Material Paneling and Carbon Layup Safety Equipment Hardware	\$716 \$229 \$46 \$50
		<b>Estimated Total</b>	<b>\$1041</b>
2	Spare Parts	Welding supplies, Hardware, Tab Materials, Tubing	\$200
3	Competition Expenses Frame Sub-team	Registration, travel (hotel rooms, vehicle rentals, gas, etc.)	\$1,125
4	Contingency (5%)	Unpredicted Expenses	\$100
		<b>Total</b>	<b>\$2466</b>

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