NPOI Nitrogen Distribution: Engineering Analysis

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November 20, 2013

Presentation Overview

- Project Description
- Nitrogen flow rate
- Tank implementation
- Tubing size & pressure drop
- Thermal expansion
- Component list
- Conclusion

Project Description

- 1000L Dewar flask supplies nitrogen to three arms of interferometer
- 30 imaging stations (6 active)
- 4 astrometric huts
- 4 sets of gate valves
- Temperature range: -20 to 120°F

Needed Flow Rate

- 2 active imaging stations
 - 2 mirror cover purges
 - 5 1in bore pneumatic cylinders
- 1 astrometric hut
 - 2 mirror cover purges
- Gate valve station
 - 3 3in bore pneumatic cylinders

Mirror Cover Purge

- 9PSI line pressure
- 0.004in diameter orifice

$$Q = CA_O \sqrt{\frac{2\Delta P}{\rho}}$$

- \bullet C= 0.75
- 0.5CFH flow rate

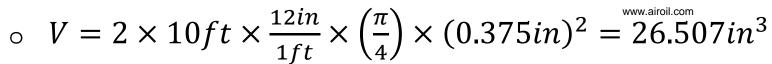


www.astronomy.net

Imaging Station Cylinders

3 in lizard head & 2 in camera dome

- Bore= 1in, stroke= 5in
- o $V = 5in \times \frac{\pi}{4} \times (1in)^2 = 3.927in^3$
- Tubes are also refilled
- D= 0.375in, Length= 10ft





Imaging Station Flow Rate

$$Q = \frac{V \times P_{abs}}{28.8 \times t \times P_{atm}} \left[\frac{in^3}{s} \right]$$

•
$$Q = \frac{30.434in^3 \times 56.3PSI}{28.8 \times 2s \times 11.3PSI} \times \frac{25}{12} = 5.484 \rightarrow 6CFH$$

•
$$P_{atm} = 11.3PSI \ at \ 7000ft$$

Gate Valves

Pneumatic cylinders operate gate valves in vacuum tubes

- Bore= 3in, stroke= 15in
- Length= 5ft
- Diameter= 0.375in

www.vatvalve.com

$$V_{cylinder} = L \times A = 15in \times \frac{\pi}{4} \times (3in)^2 = 106.03in^3$$

o
$$V_{tubes} = 10 ft \times \frac{12 in}{1 ft} \times (\frac{\pi}{4}) \times (0.375 in)^2 = 13.254 in^3$$

Gate Valve Flow Rate

•
$$Q = \frac{119.282in^3 \times 56.3PSI}{28.8 \times 2s \times 11.3PSI} \times \frac{25}{12} = 21.495 \rightarrow 22CFH$$

 Gate valves are actuated consecutively for a total run time of 6 seconds

Total Flow Rate

- Max flow rate in each arm= 25CFH
 - 6 purges= 3CFH constant flow
 - 3 consecutive gate valves= 22CFH
- Max flow rate after tank= 20CFH
 - 4 purges= 2CFH constant flow
 - 3 simultaneous actuators= 18CFH

Tank Implementation

- 5-gallon tanks will reduce load on system
- 5-gallons≅405 ft of supply tubing
- Allows gate valves to react instantly
- Reduces stress in tubing



Tubing Size

- Cleaned and capped copper tubing is available in sizes ranging from $\frac{1}{8}in$ to $1\frac{1}{2}in$
- Sizes analyzed for this project:
 - o ½in= 0.555in ID \$2.00 per ft.
 - \circ 5/8in= 0.68in ID \$2.40 per ft.



Pressure Drop Equations

- $\Delta P = \int \frac{L_{eq}}{D} \frac{\rho V^2}{2}$
- from Moody diagram using Re and (ε/D)
- L_{eq} accounts for bends, tees, and valves
- V is found using $V = \frac{Q}{A_C}$

Actual Pressure Drop

Location	Tubing ID (in)	ΔP (PSI)	Tubing ID (in)	ΔP (PSI)
Total arm (no tank)	0.555	2.9951	0.68	1.1760
Prior to tank	0.555	1.3678	0.436	4.1693
After tank	0.555	1.2872	0.436	3.9095
Main line (if feeding all 3 arms)	0.555	1.2766	0.68	0.4992
Main line (if feeding 2 arms)	0.555	1.0878	0.68	0.4260

Pressure Drop continued

- Pressure drop to manifold= 0.2751PSI
- Large ΔP= Wasted nitrogen
- Goal for $\Delta P_{max} = 5PSI$
- Actual $\Delta P_{\text{max}} = 4.2067PSI$
- Use of ½in tubing everywhere means all components will be the same

Thermal Expansion

- Change in length due to change in temperature
- Coefficient of thermal expansion for copper $\alpha = 9.3 \times 10^{-6} / {}^{\circ}F$
- Length must account for ten 180° curves and ten 45° bends
- Total length of each arm= 1113.496ft
- Longest tube= 700ft

Thermal Expansion Calculation

- $\Delta L_{hot} = L_o \alpha (T_{max} T_{install})$
- $\Delta L_{cold} = L_o \alpha (T_{install} T_{min})$
- $\Delta L_{hot} = 700 ft \times 9.3 E^{-6} (120 120)$

Thermal Expansion Stress

- Max allowable $\sigma = 6KSI$
- $\sigma = \alpha \Delta T E$
- Modulus of elasticity= 16MPSI
- $\sigma_1 = 9.3E^{-6} \times (120 70^{\circ}F) \times 16E^6$ =7.44KSI
- $\sigma_2 = 9.3E^{-6} \times (70 -20^{\circ}F) \times 16E^6$ =13.392KSI

Expansion loops

Absorbs the change in length to reduce stress

•
$$L = \frac{1}{12} \left(\frac{3E}{P} \right)^{\frac{1}{2}} (d_o \Delta L)^{\frac{1}{2}}$$

•
$$L = \frac{1}{12} \left(\frac{3 \times 16E^6 PSI}{6000 PSI} \right)^{\frac{1}{2}} (0.625in \times 7.031in)^{\frac{1}{2}}$$

• L= 16.098in

Supply Line to Manifold

- $\frac{1}{2}$ in tee(\$1.45)
- $\frac{1}{2}$ in ball valve(\$4.33)
- $\frac{1}{2}$ in tube to $\frac{1}{2}$ female NPT(\$1.79)
- $\frac{1}{2}$ in female NPT to $\frac{3}{8}$ in barb(\$3.19)
- Total cost = \$10.76

Component List

- Cleaned and capped copper tubing
 - 3700ft of ½in
- 572 fittings
- 39 manifolds
- 500ft of black PVC tubing

Conclusion

- Maximum flow rate of 25CFH
- Total pressure drop= 4.2067PSI
- Tanks will provide instant supply of nitrogen while reducing tubing size
- Expansion loops will be used to lower stress in tubing
- ½in tubing from tank to end of each arm

Questions?

References

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- 5 gallon air tank: http://www.rakuten.com/prod/5-gallon-air-tank-4-train-horn-air-suspention-more-free-gauge/248387884.html?listingld=279990422
- Tubing: http://www.lowes.com/Plumbing/Pipe-Fittings/Copper-Pipe-Fittings/Copper-Pipe-Fittings/_/N-1z10xv9/pl#