



NORTHERN ARIZONA  
UNIVERSITY  
*College of Engineering, Forestry & Natural Sciences*

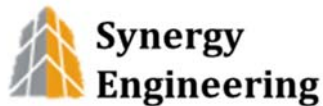
# The International Pavilion Expansion

## CENE 486C: Capstone Design

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From: Synergy Engineering

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The team would additionally like to express our gratitude to Sam Heffelfinger from Peak Engineering in assisting the team with the site design process.

Finally, the team would like to thank our instructor, Dr. Bridget Bero for all the helps throughout the project.

## 1.0 PROJECT DESCRIPTION

### 1.1 Project Purpose

The primary purpose of the project is to choose a site location for an expansion of the existing NAU International Pavilion and to design an additional building. The expansion is estimated to be 15,000 square feet. The space usage is listed below:

- 5000 square feet for classrooms
- 2000 square feet for offices
- 2500 square feet for student community space
- 3000 square feet for student study areas
- 400 square feet for the mechanical and electrical room
- 2000 square feet for miscellaneous use

Some of the building space may be dual purpose and allow for a reduced area.

### 1.2 Project Background

The existing NAU International Pavilion is located on central campus of Northern Arizona University (NAU). It is 10,000 square feet and it features student lounge space, a game area, and event space. The popularity of the existing facility has created a need for substantially more space. Therefore, Meyer Borgman Johnson Engineering requested Synergy Engineering to propose an expansion plan for an additional building at the vicinity of the existing building. The new location of the expansion would be either north, south, or west of the existing building. The east side of the building could be an option if the expansion spread over the pedestrian walkway. Figure 1.1 shows the location of International Pavilion in Flagstaff. Figure 1.2 shows the location of the International Pavilion and the surrounding buildings. Figure 1.3 shows the north elevation view of the building.

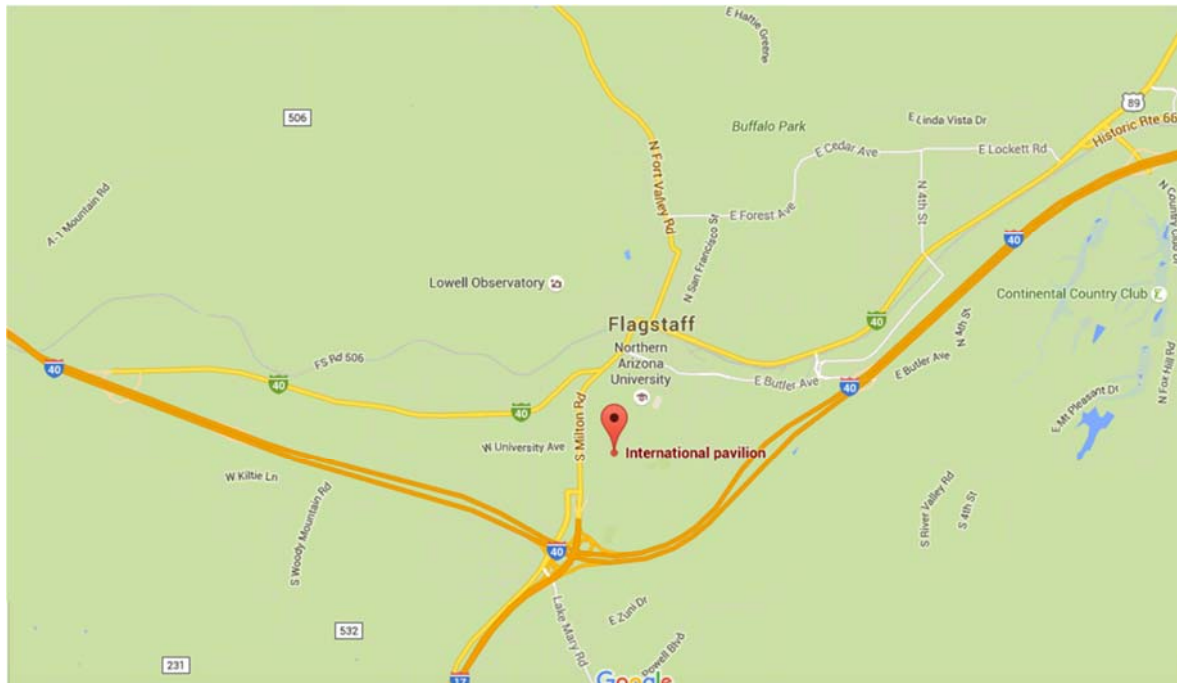


Figure 1.1 Location of International Pavilion building on Flagstaff map [1]

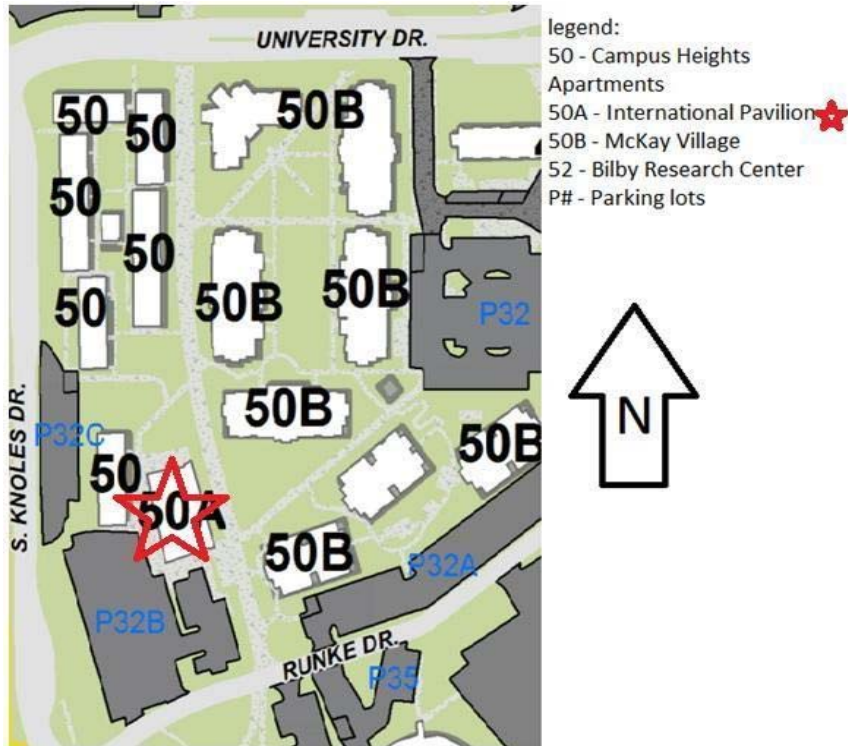


Figure 1.2 Location of International Pavilion building and the surrounding buildings [2]



Figure 1.3 North elevation view of the existing building (looking south)

## 2.0 SITE SELECTION

There are four potential site locations, which are in the south, east, north, and west of the existing International Pavilion (Building 50A) as shown in Figure 2.1. The four locations are indicated in the figure below but they are not drawn to scale.

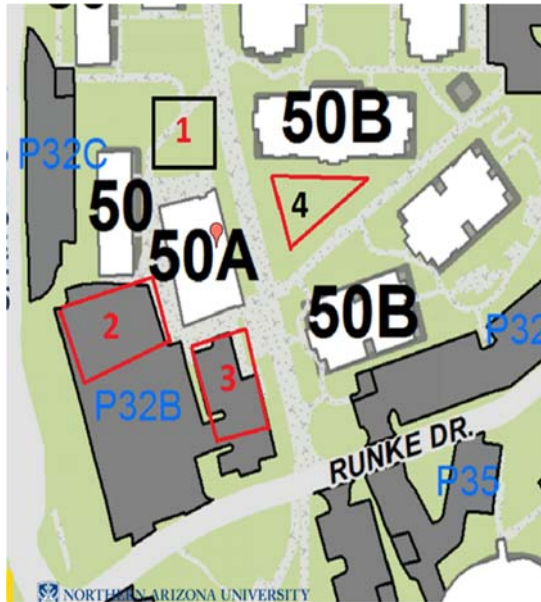


Figure 2.1 International Pavilion and four potential sites [2]

A total of seven items were considered for each site location in the decision making process. The items considered are: site elevation changes compared to the existing building, area of footprint, site utilities relocation, connection to existing building, relocation of sidewalk, removal of trees, and parking spaces taken. Table 2.1 below shows the detailed considerations for each site. EL stands for electrical line and WL stands for water line.

Table 2.1 Items considered for four sites

Items Considered	Considerations			
	Site 1	Site 2	Site 3	Site 4
Differential site elevation	-10 ft	-2 ft	+2 ft	-15 ft
Area of footprint available	10,520 sf	10,550 sf	9,020 sf	8,720-13,190 sf
Existing Utilities	Relocate detention basin, EL, 2WLs	Relocate EL and 2WLs	Relocated EL	Need no relocations
Connection to existing building	The existing pathway was considered to see if there is the potential to utilize it in the connection of the two buildings.			
Relocation of sidewalk	The existing sidewalk on the map was inspected to see if any relocation is needed. Site 4 requires a minor relocation of the sidewalk, and the other three sites requires some sorts of major sidewalk relocation.			
Removal of trees	11	0	10	9
Parking spaces taken	0	20	22	0

The following decision matrix, Table 2.2, was then created to help select the best option based on the considerations explained above. As it can be seen in the table, Site 2 and Site 3 are the better choices. The team then discuss the decision matrix and the items considerations table with the client. The client chose Site 3 because of its relatively small elevation changes

and least disruptive to existing residents in Campus Heights. Also, Site 3 has rectangular shape for a maximum use of space and it is close to the existing international building. Therefore, Site 3 was chosen for the new building. Based on the topography around Site 3, the team later decided to widen the building footprint, as can be seen in Figure 3.1. As part of the side walk relocation of sidewalk to Site 3, egress will be considered to link to the existing sidewalk.

Table 2.2 Decision Matrix for site selection

Items considered	Weight	Site 1	Site 2	Site 3	Site 4
Site elevation relative to the International Pavilion	30%	6	8	8	5
Area of the footprint	30%	7	7	7	9
Site utilities	15%	4	5	8	10
Connection to existing building	10%	7	5	8	7
Relocation of sidewalk	5%	6	6	7	8
Removal of trees	5%	5	10	6	7
Parking Spaces Taken	5%	10	6	5	10
	100%	62.5%	68.5%	74.0%	76.5%

(Scale: 1-10, 1: Bad, 10: Good)

Bad	
Neutral	
Good	

### 3.0 SURVEYING

The team surveyed around the existing building to get the influence of surrounding conditions (topography). 200 points was surveyed, which included the concrete boundary, gravels, utilities (water valves, reclaimed water valves, sewer, storm drains), fire hydrants and trees. The first control point used was the same as the point used from the existing pavilion survey. The team added another three control points in order to survey all the required points. After surveying, the team inputted the points into the Civil 3D and created a topographic map. The topographic map of the site can be found in Figure 3.1.



Figure 3.1 Topographic Map of the Site

## 4.0 DESIGN DOCUMENTS REVIEW

### 4.1 Geotechnical Reports Review

Speedie & Associates prepared the geotechnical reports for the vicinity of the International Pavilion in 2013 [3]. They did the soil borings and made recommendations for the International Pavilion. The team reviewed the existing soil report for the International Pavilion to obtain the information that is relevant to the expansion project. The soil profile for new building is as shown in the Figure 4.1. There is no groundwater present in the site location. The subsoil at the site is suitable for support of the proposed structure spread footings bearing on the weathered limestone. The area is located in a seismic zone that is considered to have low to moderate historical seismicity. Site class definition, Class B, which is the educational occupancy for students, may be used for design of the structures. The foundations may bear on properly compacted engineered fill at a minimum depth of 30 inches below finished exterior grade. The allowable bearing capacity of 3,500 psf can be utilized for design and the bearing capacity refers to the total of all loads, dead and live, and is a net pressure. It may be increased one-third for wind, seismic or other loads of short duration. Continuous wall footings and isolated rectangular footings should be designed within widths of 16 and 24 inches respectively. Continuous footings and stem walls should be reinforced to distribute stresses arising from small differential movements, and long walls



should be provided with control joints to accommodate these movements. Reinforcement and control joints are suggested to allow slight movement and prevent minor floor slab cracking. Lightly loaded interior partitions (less than 800 plf) may be supported on reinforced thickened slab sections (minimum 12 inches of bearing width). [3]

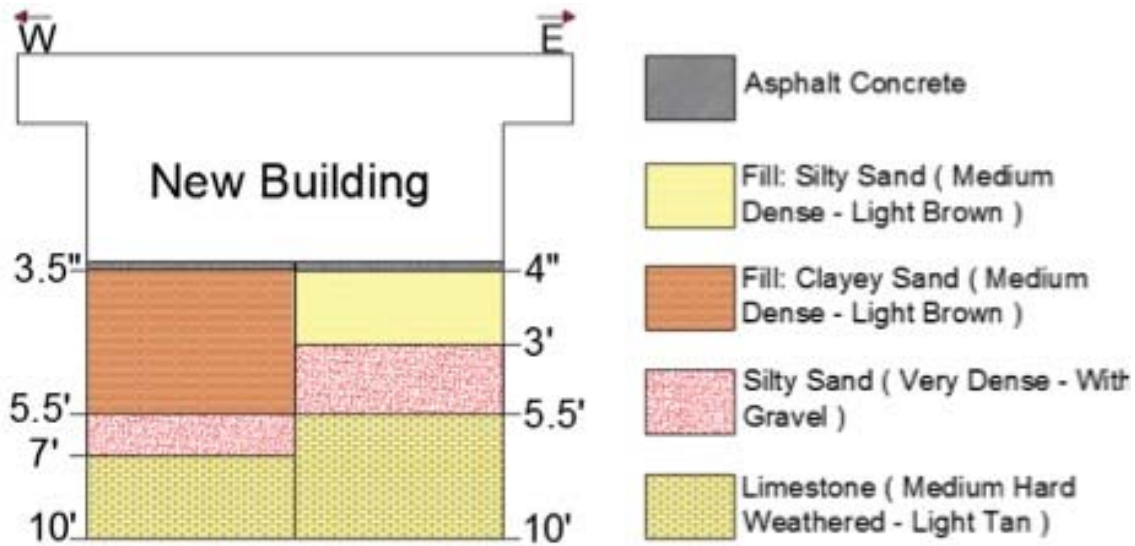


Figure 4.1 Soil Profile for new building

#### 4.2 NAU Technical Standards Review

NAU Technical Standards is an internal document that applies to NAU properties only. The requests of building code variance, the functions of proposed building including building entrance, flood prevention, ramps and curb ramps were discussed in the NAU technical standard. Also, if any conflicts occur in the design guidelines or in the Technical Standards, the team shall follow the applicable building codes.

- *The requirements in this document do not supersede any applicable building codes. These requirements are in addition to all applicable codes, ordinances, statutes, regulations, and laws. If there is a conflict with any requirements in the design guidelines or in the Technical Standards, the applicable building codes take precedence [4].*
- *Requests for variance shall be evaluated by the NAU Fire Marshal (NAUFM) staff and NAU Building Official (NAUBO) staff, to ensure the proposed design, use, or operation satisfactorily complies with the intent of the IFC, IBC with related codes and NAU Technical Standards, as adopted by Northern Arizona University (Building Code Variance Requests*
- ) [4].

- *The main entrance of a building shall be universally accessible via a single route. All building entrances shall be accessible - including employee entrances or entrances other than the main entrance (Section 2 - Accessible Routes- Building Entrances) [4].*
- *Where changes in elevation are encountered (including courtyards and open spaces) full consideration shall be given to university accessible design that addresses elevation change.*
- *Where grades/space allow, sloped sidewalks (slope 1:20 or flatter) shall be used to overcome changes in elevation.*
- *Ramps (defined as anything steeper than 1:20 slope) shall have a maximum of 1:16 slope (Section 2 - Accessible Routes- Ramps) [4].*
- *Curb ramp slopes shall be 1:12.*
- *Concrete aprons shall be provided at the bottom of the curb ramps.*
- *Curb ramps within sidewalks (parallel to the path of travel) shall be provided with a 1:16 slope.*
- *The University's standard for detectable warning surfaces is truncated domes in a contrasting color.*
- *The depth of detectable warning surface in the direction of travel shall not exceed 24 inches (Section 2 - Accessible Routes - Curb Ramps (curb cuts)) [4].*
- *Proposed building ground floor elevations and any apertures into the building should be 1 feet or more above the 100-year floodplain. Sunken access ways or patios leading to building levels below the natural grade of the site are not permitted when adjacent to a 100-year floodplain, and discouraged in other areas. Soil should be graded so that water drains away from the building at a minimum of 2%, subject to other site criteria, such as accessibility. Elevations of underground utilities shall be considered in the grading layout (Section 6 - General Storm Water Guideline -Flood Prevention) [4].*

### **4.3 The City of Flagstaff Engineering Standards Review**

The City of Flagstaff Engineering standards covers the items to focus in the soil report, mapping requirements, easement requirements, fire access requirements, and context sensitive design requirements. However, it is not mandatory for NAU to follow the City of Flagstaff Standards due to NAU is a federal property. The team review the city standards to check for its discrepancies with the NAU technical standards and the International Building Code. Also, it serves as a guideline for things to be aware of in the designing process

- *The soils engineer shall address the following problems: shrink-swell potential, ground water, wetness, depth of rock, erosion, flood hazard, allowable velocity in earth drainage channels, bearing capacity, corrosion potential, organic layers, ease of excavation, and*

*other pertinent issues. Correlated “R-values” that are used in the pavement structural section design should be determined from soil samples containing the highest amount of clay (PI values).*

- *If higher PI values are reported but not considered in the determination of the correlated R-values, the engineer shall provide recommendations for removal of these materials, including specific areas of removals that must be reflected on the approval civil plans.*
- *If cut and fill slopes are proposed which exceed those allowed by City standards and/or Flagstaff City Code Title 4, Building Code, a slope stability analysis establishing maximum stable slope grades must be included (Section 13-05-001-0002 Soils Report) [5].*
  
- *A complete boundary survey based upon fieldwork shall be performed prior to submittal of the preliminary plat, and documentation of said survey shall be included with that submittal.*
- *Mapping (including contours) of the site and adjacent areas shall be sufficient to show clearly the influence of surrounding conditions (topography) as well as the influence of the proposed development on surrounding conditions.*
- *Contour interval shall be one foot or two feet, depending on the slope of the ground and the judgment of the Engineer or Land Surveyor (Section 13-02-001-0001 Mapping) [5].*
  
- *The City of Flagstaff Utilities Division requires safe and quick access to all city water and sewer mains at all times in order to repair main breaks, install taps, and perform preventive maintenance. For this reason, City of Flagstaff water and sewer mains shall be constructed in streets within the public right-of-way. Where possible, water shall be 10 ft. north or east of centerline and sewer on the centerline. Water mains in easements create access problems and will not be permitted except under the following special circumstances.*
- *When a water or sewer main is located adjacent to a building, the main shall be offset a minimum of ten (10) feet from the building in a minimum twenty (20) foot easement (Section 13-09-001-0008 Utility Alignment and Easement Requirements) [5].*
  
- *A fire access drive 20 feet in width minimum, with 13 feet 6 inches of overhead clearance will be required within 150 feet of all buildings. 1. Fire access drives 26 feet in width minimum (measured from the eave or flat roof parapet) will be required for structures 20 feet high or greater. 2. Access for up to two single-family dwelling units may be supplied by a 10-foot wide driveway meeting all Fire Department requirements.*
- *If the access drive exceeds 150 feet in length and is not looped, an approved turn-around shall be supplied. (Section 13-13-004-0001 Fire Access) [5].*
  
- *Baseline Design Theme Preservation of, and compatibility with, Flagstaff’s natural environment is the baseline design theme. Landscape designs shall maximize the amount of land retained in its natural state. Projects shall be designed to preserve and protect*

*native vegetation, particularly existing trees and attractive natural features. New landscaping for rights-of-ways shall seek the restoration of the natural environment disturbed by construction. The baseline theme may vary depending on location and use. (13-18-002-0003.1 Context Sensitive Design) [5].*

#### **4.4 International Building Code (IBC) 2012 Review**

The team used international building Code 2012 as a backbone for the structural design portion of the proposed building.

- The proposed building height was classified as type I or II (Chapter 5 General building heights and areas: Table 503 in Section 602) [6].
- The building occupancy was classified as Businesses Group B. (Chapter 5 General building heights and areas: Section 302) [6]
  
- Building element shall have fire-resisting material as shown below:
  - Primary structure frame 2 hours
  - Bearing wall 2 hours
  - Non-bearing wall is separated by distance, then fire resisting shall need to restrain 1 hour
  - Interior 0 hour
  - Floor 2 hours
  - Roof 2 hours
  - If building is: Type I: h=160 ft, A=Unlimited, 11 stories  
Type II: h=55 ft, A=23,000 ft<sup>2</sup>, 3 stories (h=height, a=area)  
(Chapter 5 General building heights and areas: Section 602)
- Yards and other spaces for any system that belongs to the buildings shall be included in building perimeter. (Chapter 5 General building heights and areas: Section 5.7) [6].
  
- Table 1604.3 of the Structural design chapter illustrates the deflection limit in members, which should not be exceed in designing. The table demonstrates the limits for roof members, floor members, and exterior walls and interior portions. This table also provides the limits due to snow, wind, live, and dead loads [6].
  
- The risk category, which requires in the structural elements design, was classified as category III based on the occupancy. the category was chosen based on the listed criteria :“Building and other structures containing adult education facilities, such as colleges and universities, with an occupant load greater than 500” (Chapter 16 Structural Design: Table 1604.5).
- Load Combinations formulas will be used in the required load calculations. These formulas include dead, live, snow or rain, and wind loads. (Chapter 16 Structural Design: Table 1605.2) [6].

- Minimum live loads and the reduction factors can be found in Table 1607.10.1 and Table 1607.10.1. The reductions factors can be used to reduce loads that structural members have to support.
- Due to the weather of flagstaff, snow load has to be considered. Section 1608 will provide the minimum snow load that shall be consider in the design.
- The structural design portion will be based on the formulas and tables from ASCE 7-10. (Chapter 16 Structural Design) [6].
- Chapter 18 Soil and foundations, is a guidance of what kind of foundation to select, along with any necessary additions to the foundation [6].

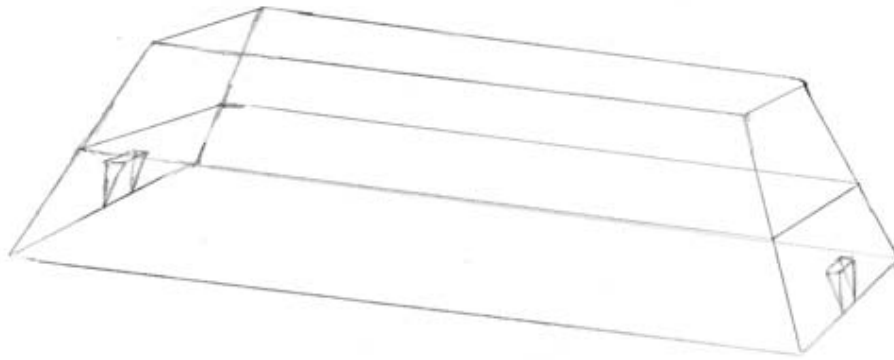
## **5.0 STRUCTURAL DESIGN**

### **5.1 Building Layout Options**

In this project, in order to start the design process, a building shell need to be established. After a building shell is selected, a framing plan of the building can be determined. For this task, the team designed four different shell models with a propose of fulfilling the requirements as requested by the client:

- Classroom – 5000 sf (800-1000 sf)
- Office – 2000 sf
- Student community space – 2500 sf
- Student study area – 3000 sf
- Mechanical / electrical – 400 sf
- Misc – 2000 sf
- Building height of 40 ft.
- Distance between the existing and proposed building is minimum 30’.

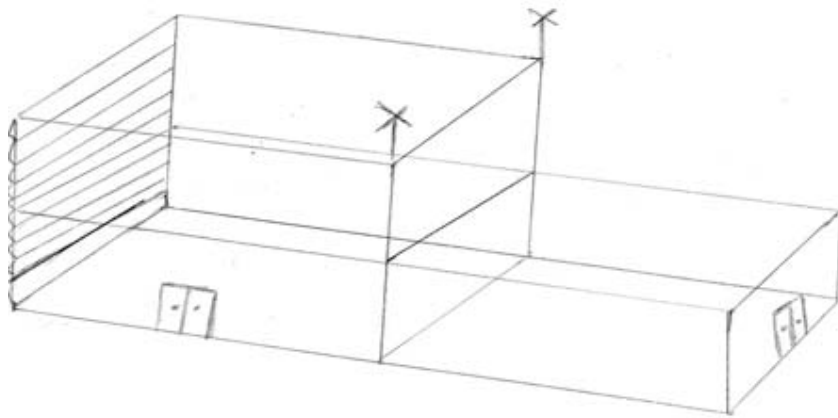
The first building shell is as shown in Figure 5.1. It was inspired by the Egyptian pyramids shape and its stability throughout the thousands of years. Also, the second reason to choose this is that the angled wall, similar to the what was utilized by the Egyptian, it is stable for its shape [7].



Design 1

Figure 5.1 Building Shell Option 1

Figure 5.2 below shows the second proposed building shell. The shell basically mirrors the rectangular shape of the existing pavilion, but with an added open area on the second floor. This design provides more nature fresh air to the space and for people to socialize. In addition, the shape of the shell will maximize the wind energy and solar energy usage. In the idea, windmills can be installed on top of the left side building, and solar panels can be mounted on the windows of the building.

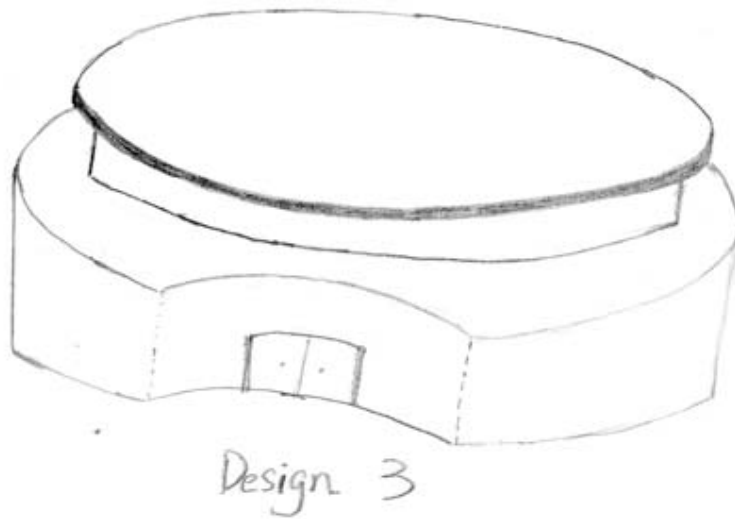


Design 2

Figure 5.2 Building Shell Option 2

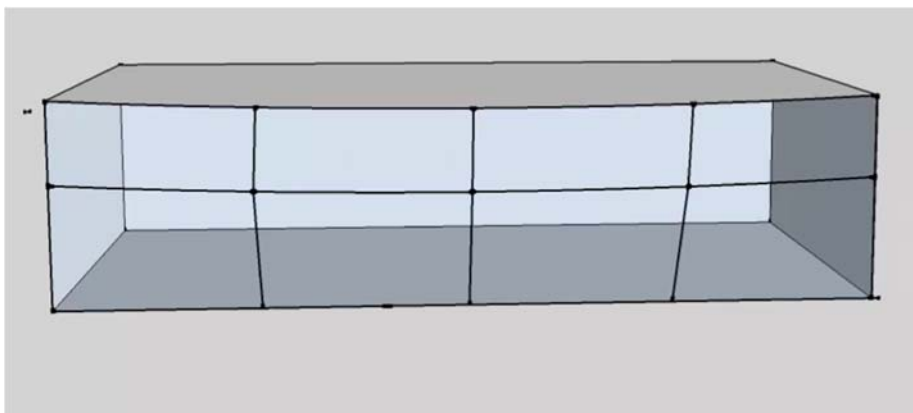
The concept for third building shell was based on a tradition Chinese dwelling, the Fujian Tulou, to incorporate the cultural exchange idea, to attract attention, and to make it easier to be recognized among the neighboring buildings. The Fujian Tulou are Chinese rural dwellings unique to the Hakka in the mountainous areas in southeastern Fujian, China. They

were mostly built between the 12th and the 20th centuries. It is usually a large, enclosed and fortified earth building, most commonly rectangular or circular in configuration, it can house up to 800 people. Smaller interior buildings are often enclosed by these huge peripheral walls which can contain halls, storehouses, wells and living areas, the whole structure resembling a small fortified city [8]. The below figure shows the design of the building based on the idea of the Fujian Tulou.



*Figure 5.3 Building Shell Option 3*

The fourth proposed building shell shown in Figure 5.4 and Figure 5.5 utilizes the simple rectangular shape and sloped window based wall in the south side of the building. It does not have a much too fancy shape, which makes it easier to incorporate energy-saving, and environment adaptation ideas. The team also discussed the advantages and disadvantages of the shell in either North and South, or East and West orientations.



*Figure 5.4 Building Shell Option 4 (front view)*

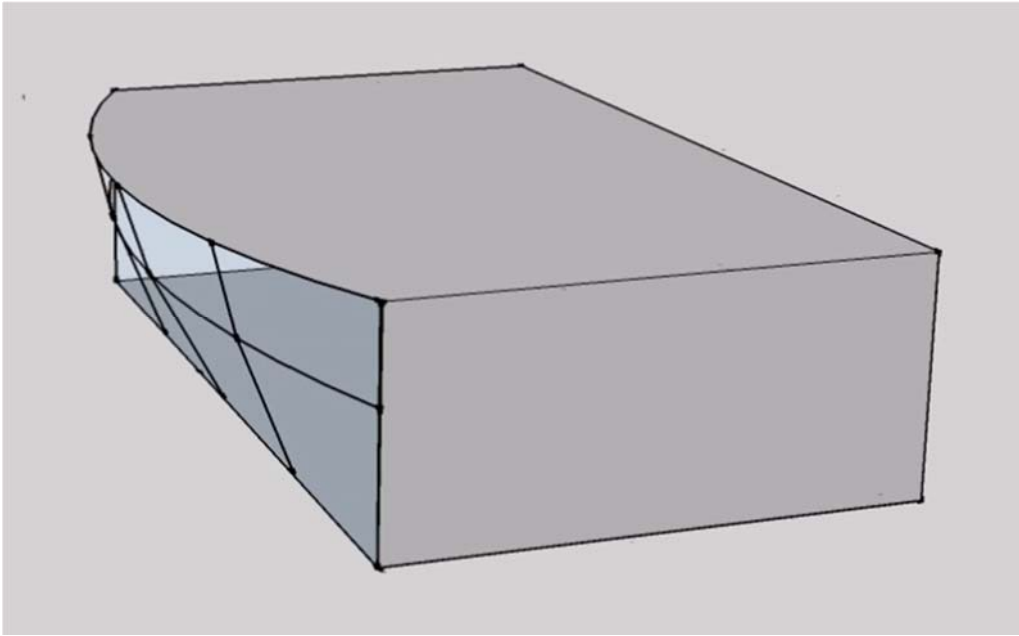


Figure 5.5 Building Shell Option 4 (side view)

Option 4 was established based on the previous three options in the two meetings with Prof. Alan Francis along with our advisers Dr. Robin Tuchscherer and Prof. Kai Kaoni. The five design principles that were used in establishing the final design are:

- Culture Exchange
  - As International Pavilion is a dynamic event destination for all the students in NAU, it allows different nationalities to gather, interact with each other, and exchange their cultures.
- Energy Saving building
  - The building will need to provide alternative green energy solutions along with providing an efficient heating and cooling systems.
- Connection with the existing building
  - As the new building is the expansion of the existing International Pavilion, the two buildings need to connect in some ways.
- Have all the necessary spaces
  - This means that the required spaces should all fit in the proposed design.
- Central innovation side of Campus as indicated in NAU Master Plan
  - This principle focus on the design and it should be creative and modern as the NAU ambition towards the future of this section of the campus.

In Option 4, the first and fourth principle was achieved as shown in the floor plan in Figure 5.6. It provides an adequate space for the socializing and meetings. In order to be an energy-saving building, the team will design the structural frame to carry the solar panels loads on the roof. Also, one of the reasons to choose angled glass wall is to provide passive heating in the wintertime, which will keep building warm and to prevent excessive heat entering during



the summer days. Because of the design distance between the existing building and the proposed one, the team suggests a covered sidewalk between them to provide open air social areas during the summer days, and prevent the accumulation of excessive snow during winter. Finally, the building shell is an innovative design and requires structural cantilever to complete the design, which satisfy the challenges set forth in the NAU Master Plan.

After establishing Option 4 as the final design, the floor plan was created according to the space usage provided by the client. The floor plan can be seen below in Figure 5.6.

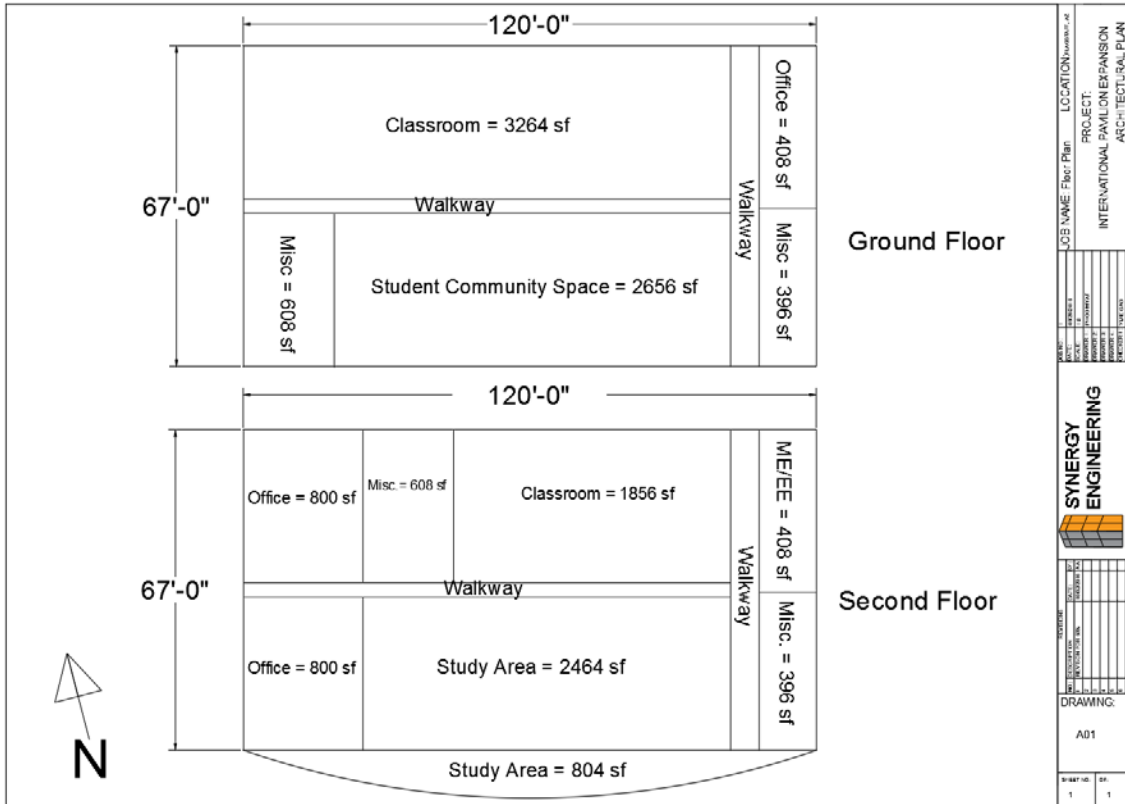


Figure 5.6 Floor Plan

## 5.2 Framing Plan and Details

This section will illustrate the building's framing plan based on the chosen shell.

### 5.2.1 Preliminary Framing Plan

Figure 5.1 illustrates the preliminary framing plan for the ground floor of the building. The spacing between the columns is used as the recommended conservative choice based on the advice from our technical advisor.

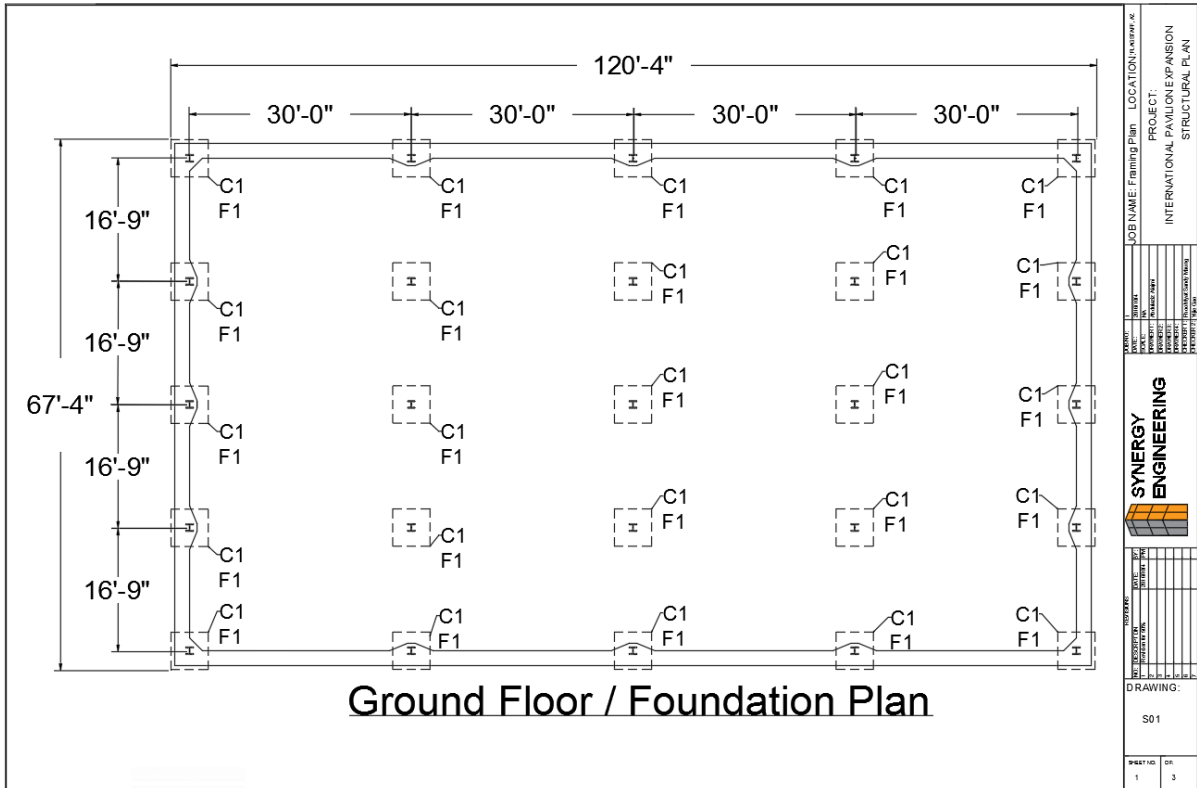


Figure 5.6 Preliminary Framing Plan (Ground Floor)

For the second floor framing plan in Figure 5.7, a slab-based floor was utilized to reduce the vibration of the steel frame chosen. In the roof framing plan, the floor system will be a joist-based system because there will not as much vibration as the second floor. The framing plan for roof can be seen in Figure 5.8.

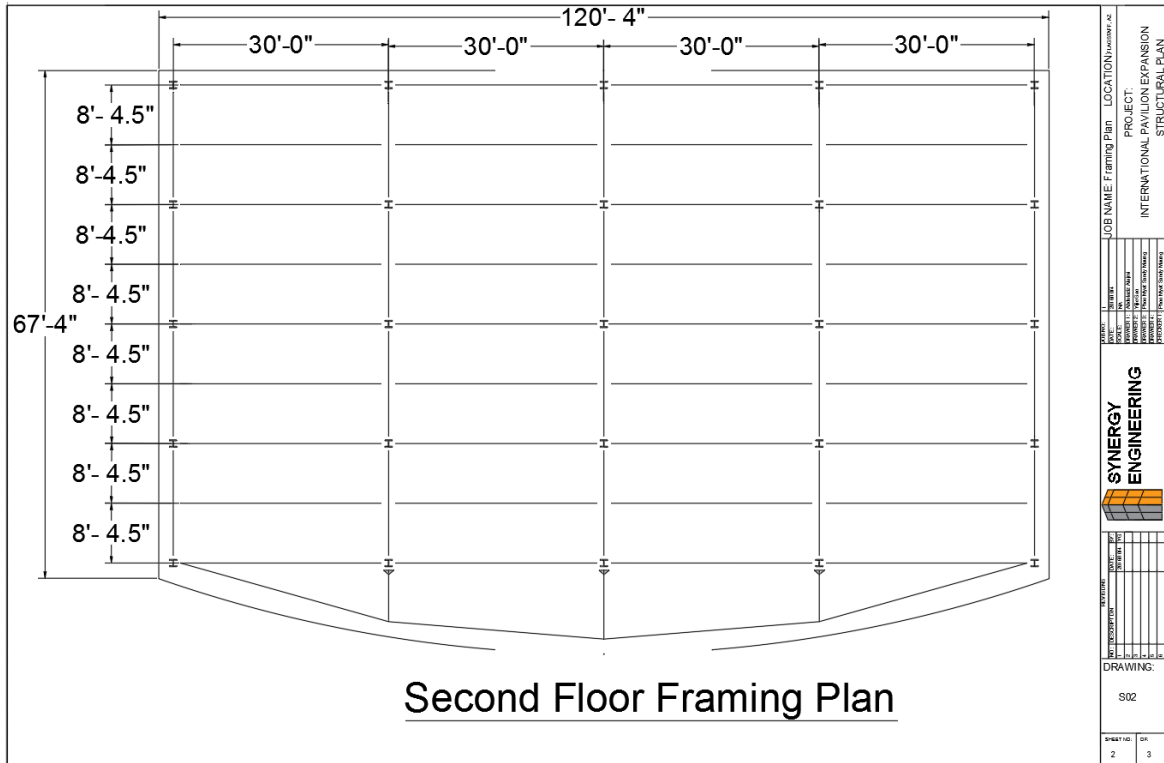


Figure 5.7 Preliminary Framing Plan (Second Floor)

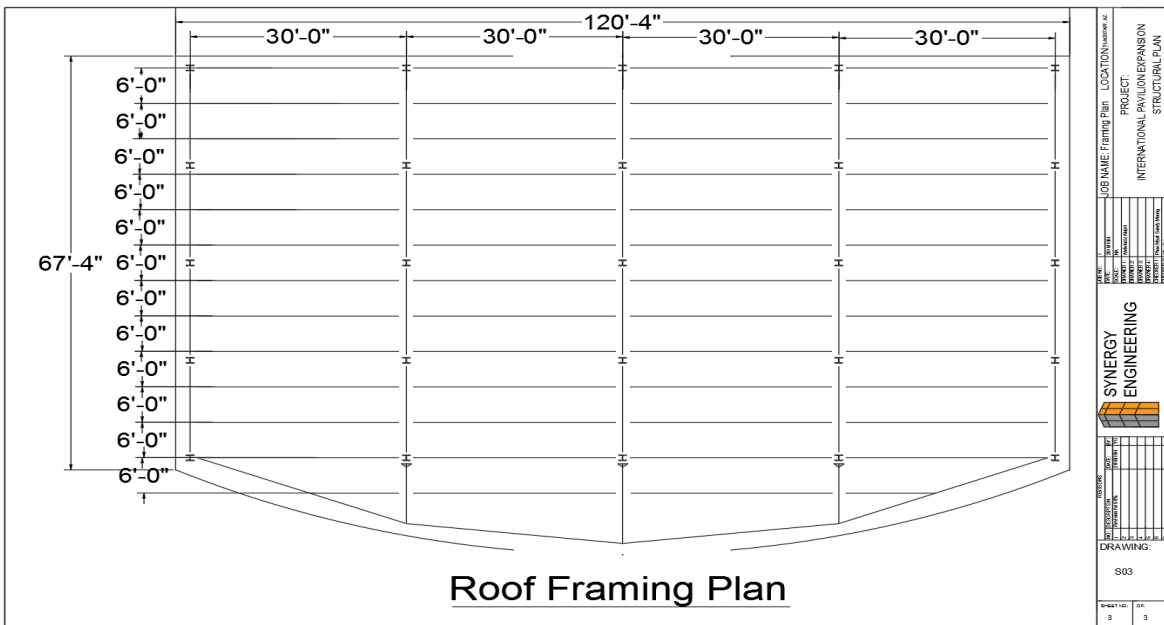


Figure 5.8 Preliminary Framing Plan (Roof)

### 5.2.2 Design Loads

The following loads have been calculated so that the team can move forward the framing portion of the design process.

- *Live Loads*

The live load was calculated from ASCE 7-10 based on the space usage of the proposed building [9]. The calculation can be found in Appendix 8.1. All of the live load listed will be used in the structural design portion and will allow for reduction or construction easement accordingly.

- *Dead Loads*

(In process)

- *Snow Loads*

The snow loads are calculated based on the roof slope, shape, thermal properties, and a percentage of ground snow loads. ASCE 7-10 was used to determine the ground snow load, and the different factors [9]. The snow load was calculated to be 38.5 psf. The detailed calculation can be seen in Appendix 8.2.

- *Seismic Loads*

(In process)

- *Wind Loads*

The wind loads are calculated based on the basic wind speed, occupancy category, importance factor, exposure category, gust effect, and internal pressure coefficient. ASCE 7-10 was used to determine the basic wind speed, and the different factors [9]. The wind load was calculated to be 23 psf for the roof, 23psf in the windward direction and 9 psf in the leeward direction.

## 5.3 Foundation Plan and Details

## 5.4 Earth Retention Structures

## 6.0 CONSTRUCTION COST ESTIMATE

## 7.0 REFERENCES

- [1] "Google Maps", Google Maps, 2016. [Online]. Available:  
[https://www.google.com/maps?ion=1&espv=2&q=northern+arizona+university&bav=on.2,or.r\\_cp.&biw=1242&bih=585&dpr=1.1&um=1&ie=UTF-8&sa=X&ved=0ahUKEwinh9-Y4\\_vLAhVX6GMKHVEjDAsQ\\_AUIBygC](https://www.google.com/maps?ion=1&espv=2&q=northern+arizona+university&bav=on.2,or.r_cp.&biw=1242&bih=585&dpr=1.1&um=1&ie=UTF-8&sa=X&ved=0ahUKEwinh9-Y4_vLAhVX6GMKHVEjDAsQ_AUIBygC).
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- [9] ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, 2010

## 8.0 APPENDICES

### 8.1 Live Loads Calculation

Roof (Reducible): 20psf

Hanging Catwalks: 40psf

Floors:

Classrooms: 40psf

Student community space: 100psf

Student study area: 60psf

Offices: 80psf

Office Concentrated Load: 2000lbs

Partition: 0 psf (not required where the minimum specified live load >80psf)

Light Storage: 125 psf

Partition: 0 psf

Lobbies and first floor corridor: 100psf

Corridor above first floor: 80psf

Stair: 100psf

Stair Tread Concentrated Load: 300lbs

Catwalks: 75psf

Mechanical Rooms: 125psf

### 8.3 Snow Loads Calculation

Ground snow load ( $P_g$ ) = 50 psf

Exposure factor ( $C_e$ ) = 1.0 (partially exposed)

Thermal factor ( $C_t$ ) = 1.0

Importance factor (I) = 1.1 (category III)

Warm roof slope factor ( $C_s$ ) = 1.0

Flat roof snow load ( $P_f$ ) =  $0.7C_eC_tC_sIP_g = 38.5$  psf

### 8.5 Wind Loads Calculation

Basic wind speed = 120 mph

Occupancy category = III

Importance factor (I) = 1.1

Exposure category = C

Gust effect factor = 0.85 (rigid building)

Internal pressure coefficient ( $G_{cpi}$ ) = +/- 0.18 (enclosed building)  
 $K_z = 0.98$ ,  $K_{zt} = 1$ ,  $K_d = 0.85$

$$q_z = 0.00256K_zK_{zt}K_dV^2 = 34 \text{ psf}$$

Windward:

$$C_p = 0.8$$

$$\text{Windward} = q_z G C_p = 34 * 0.85 * 0.8 = 23 \text{ psf}$$

Leeward:

$$C_p = -0.3$$

$$\text{Leeward} = 34 * 0.85 * 0.3 = 9 \text{ psf}$$

Roof:

$$C_p = -0.9$$

$$\text{Roof} = 34 * 0.85 * 0.9 = 26 \text{ psf (upward)}$$